NATIONAL BUREAU OF STANDARDS REPORT

4038

THERMAL CONDUCTIVITY OF A SPECIMEN OF INCONEL

bу

Lloyd E. Richards Henry E. Robinson

Report to

Argonne National Laboratory Lemont, Illinois



U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS

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Heating and Air Conditioning Section Building Technology Division

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I Introduction

A specimen, designated as Inconel, was submitted by the Argonne National Laboratory of Lemont, Illinois for measurements of thermal conductivity.

II Preparation of the Specimen

The general arrangement of the test apparatus is shown in Figure 1.

The lower end of the specimen was heated by an electrical heating element inserted in the lower well of the specimen; the upper end was cooled by water circulated through the upper well. The heating element, having about 56 ohms resistance, was made by passing nichrome wire through a multiple hole porcelain cylinder 1/2 inch in diameter. Chromel-alumel thermocouples were attached at intervals of about 4 cm. along the length of the bar by peening the junctions into one-millimeter radial holes about 2 mm deep in the side of the specimen. An additional thermocouple was attached to the lower end of the specimen. The specimen was supported on a thin nichrome pin located in the bottom of a thick-walled stainless steel guard cylinder. The guard cylinder was also equipped with a heater element and cooling coil and with thermocouples at appropriate positions.

The specimen-guard assembly was suspended in a large sheet-metal container and the entire system insulated with a fine granular insulation of known thermal conductivity characteristics.

III Test Method

Electrical energy from a d.c. source was supplied to the heater elements and adjusted so that a minimum temperature difference between bar and guard existed at the thermocouples just above the heaters. Cooling water at a constant temperature of about 40°C was pumped through the well in the speciment and through the coil on the guard. When steady temperature conditions had been attained, the emf's of the thermocouples and the current through and voltage drop across the



bar heater were measured by means of standard resistors and a precision potentiometer. Temperature conditions were considered satisfactorily steady when no thermocouple on the bar changed temperature at a rate greater than 0.5 degree C per hour; several readings taken over a period of three or more hours after steady condtions were attained were averaged for each test.

To calculate the thermal conductivity, the observed temperatures of the bar and guard were plotted versus position along the bar as abscissae and smooth curves were drawn through the points. Corrections to the measured heat input to the bar to account for heat interchange between the bar and guard were made on the basis of the temperature differences between them determined from the curves and using the thermal conductance of the granular insulation at the appropriate mean temperature. The corrections were made for the heat interchange (a) between the lower end of the bar and the guard, (b) between the bar and guard at the heater region and (c) between bar and guard for each thermocouple span. The average rate of heat flow between any two adjacent thermocouples on the bar was thus computed and used, together with the measured distance and temperature difference between them and the cross-sectional area of the specimen, to calculate the average thermal conductivity for that span.

The maximum difference for any thermocouple span between the computed heat flow in the span and the measured electrical input to the heater ranged from 0.3 to 9.2 percent of the input, in the various tests. It is believed that since the calculated values of heat interchange could be evaluated with an uncertainty of not more than 20 percent, the uncertainty in the rates of heat flow used in computing the thermal conductivities were of the order of not more than 2 percent.

For each of the separate tests, the thermal conductivity was computed for each of the six thermocouple spans on the bar, corresponding to the mean temperature existing in each span.

IV Test Results

The values of thermal conductivity obtained for each test span were plotted against their corresponding mean temperature, as shown in Figure 2, and are represented by a curved line drawn through the plotted values. The line was determined by fitting a quadratic equation to the data.



Table 1 lists thermal conductivity values for various mean temperatures, as taken from the curve.

V Discussion of Results

The plotted points show some scatter from the curve. Such scatter is an inverse measure of the precision of the measurements, as affected by such factors as small random inaccuracies in determining the thermocouple locations on the bar, slight heat conduction along the thermocouple wires near the hot junctions, and possible slight inhomogeneities in the thermocouple wires. To minimize heat conduction effects, the thermocouple wires were led away from the hot junctions and wrapped around the bar for a few centimeters in the plane of its cross section, in which the temperature should be fairly uniform. However, since the temperature gradients along the bar ranged from 11 to 33 degrees C per centimeter in the several tests, some conduction effect on individual thermocouple readings probably could not be avoided.

Since the factors involved in inaccuracies in measurements of thermocouple positions and temperatures were random in nature, their effect was probably to decrease the precision of the values obtained for each span rather than to affect the overall results in any one direction.

Test number one was found to give thermal conductivity values materially higher than the other five tests so it was not used in the calculation of the curve in Figure 2. This shift of thermal conductivity with time seems to be an effect of the thermal history of the specimen, and has been observed in similar magnitude in several other measurements made on Inconel. It may be of interest that the data for test number one were taken less than 24 hours after first heating the specimen and that for test number two about 48 hours after that for test number one.

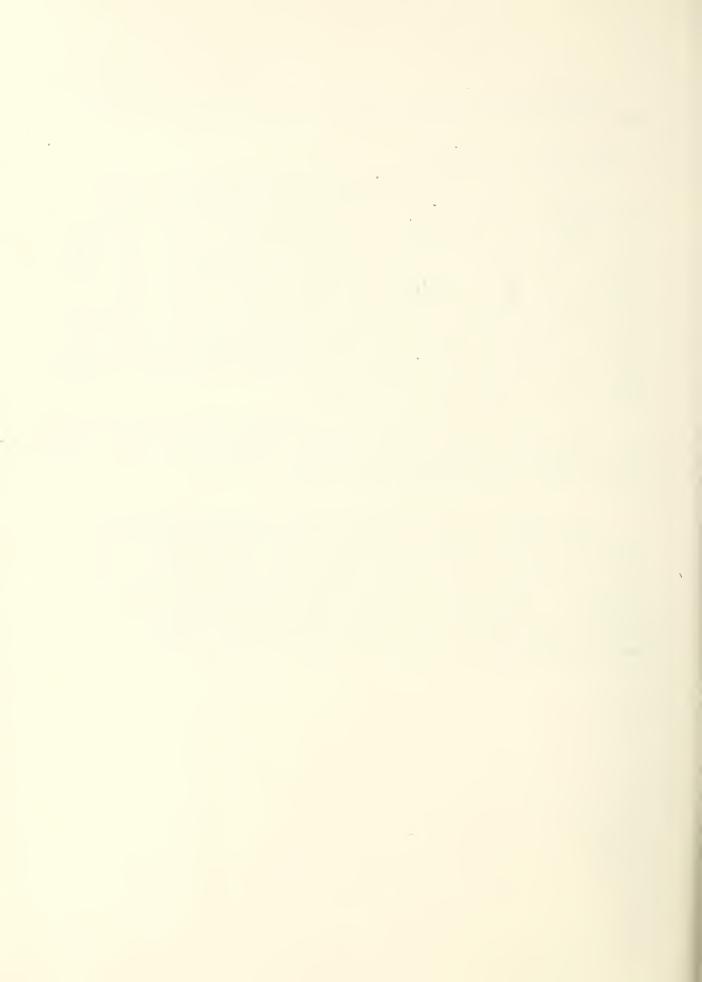
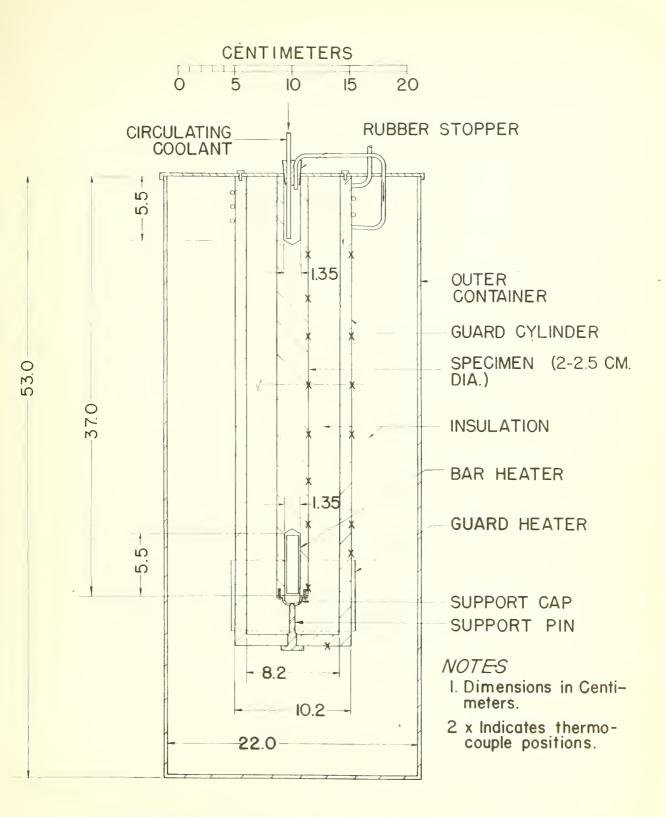


TABLE I

INCONEL

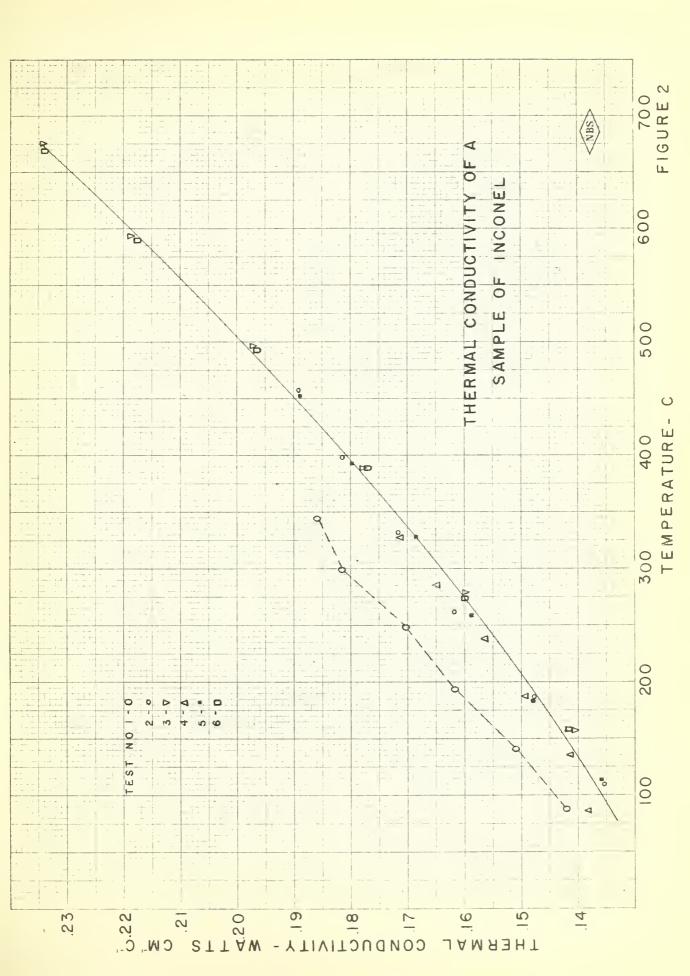
Mean Temperature (C)	Thermal Conductivity (Watts cm ⁻¹ C ⁻¹)
100	0.136
200	0.149
300	0.164
400	0.180
500	0.198
600	0.218
700	0.240





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Information on the Bureau's publications can be found in NBS Circular 460, Publications of the National Bureau of Standards (\$1.25) and its Supplement (\$0.75), available from the Superintendent of Documents, Government Printing Office. Inquiries regarding the Bureau's reports and publications should be addressed to the Office of Scientific Publications, National Bureau of Standards, Washington 25, D. C.

