

NASA/TM-2014-218513



# Data Reduction Functions for the Langley 14- by 22-Foot Subsonic Tunnel

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August 2014

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Space Administration

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August 2014

Available from:

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## Table of Contents

Abstract .....	1
Introduction .....	1
Engineering Units' Conversions .....	2
ASIN .....	2
LIN .....	3
POLY .....	4
TYPE_J .....	5
Tunnel Parameters .....	6
Flowmeters .....	11
Jet Exhaust Measurements .....	12
Balance Loads and Model Attitudes .....	19
Initial Loads .....	20
Second Order Interactions Due to Initial Loads .....	21
First and Second Order Balance Interactions .....	22
High Interactions and High Model Restraints .....	23
Air Line Pressure Corrections .....	25
Sting Deflections .....	27
Weight Tares .....	29
Method of Attachment .....	31
Angles' Calculations .....	32
Rotation of Angles from Gravity Axis to Balance Axis .....	33
Rotation of Angles from Gravity Axis to Model(Body) Axis .....	35
Rotation of Angles from Wind Axis to Gravity Axis .....	36

Rotation of Angles from Wind Axis to Model(Body) Axis .....	37
Balance Axis Angles .....	38
Model(Body) Axis Angles .....	40
Model Height .....	42
Balance Components Rotated & Translated to Model Axis .....	43
Apply Estimates of Heyson's Boundary Interference – Walls Up .....	45
Apply Estimates of Heyson's Boundary Interference – Walls Down .....	47
Blockage and Jet Boundary Corrections .....	49
Heyson's Boundary(Wall) Interference Functions .....	51
Heyson's Boundary(Wall) Interference Function 2 - Average Wind Tunnel Interference Over a Swept Wing .....	53
Base(Cavity) Pressures .....	56
Model Axis Components and Coefficients .....	59
Stability Axis Components and Coefficients .....	61
Wind Axis Components and Coefficients .....	63
Reference Axis Components and Coefficients .....	65
Model and Wall Pressures .....	67

## **Abstract**

*The Langley 14- by 22-Foot Subsonic Tunnel's data reduction software utilizes six major functions to compute the acquired data. These functions calculate engineering units, tunnel parameters, flowmeters, jet exhaust measurements, balance loads/model attitudes, and model /wall pressures. The input(required) variables, the output(computed) variables, and the equations and/or subfunction(s) associated with each major function are discussed.*

## **Introduction**

In the Langley 14- by 22-Foot Subsonic Tunnel, data acquisition consists of analog, digital, pressure, and automated cart data. Analog and digital data is acquired with the NEFF 600, pressure data is acquired with the ESP 8400, and automated cart data is acquired using the Channel Access software package. After data acquisition, data reduction functions are utilized to compute engineering units, tunnel parameters, flowmeters, jet exhaust measurements, balance loads/model attitudes, and model /wall pressures. For consistency, the names written to an online output data file are used as much as possible in this document. All calculations are single precision except where noted.

## Engineering Units' Conversions

Analog channel data is acquired and converted to millivolts. Next, the data is converted to engineering units. The engineering units' conversions commonly used in the 14- by 22-Foot Subsonic Tunnel for analog data are *asin*, *lin*, *poly*, and *type\_j*.

### ASIN

\* **Equation Definition**  
value = ( (chan#### - chan####<sub>woz</sub>) - bias ) / sensitivity  
if (value > 1.0) then  
value = 1.0  
if (value < -1.0) then  
value = -1.0  
eu = ( dasin(value) \* 57.2957795131 ) - offset

\* **Setup Example**  
name,FALPHA chno,3 dau,Neff  
desc,Model pitch  
units,deg  
euconv,asin  
lce(1.233,260.45,-0.102)  
range,160  
filter,1  
cmplmt,-10  
cmpulmt,10  
dztype, no

\* **Equation Example**  
value = ( chan0003 - 1.233 ) / 260.45  
if (value > 1.0) then  
value = 1.0  
f (value < -1.0) then  
value = -1.0  
FALPHA = ( dasin(value) \* 57.2957795131 ) + 0.0102



## LIN

### \* *Equation Definition*

$$\text{eu} = ( (\text{chan#####} - \text{chan#####}_{\text{woz}}) \\ * ( \text{expected power supply voltage} / \\ \text{actual power supply voltage} ) * \text{sensitivity} ) + \text{offset}$$

### \* *Setup Example 1*

name,TA chno,1 dau,Neff  
desc,tunnel ambient temperature  
units,degf  
euconv,lin  
lce(0.036,-40)  
range,5120  
filter,1  
dztype, no

### \* *Equation Example 1*

$$\text{TA} = ( \text{chan0001} * 0.036 ) - 40.0$$

### \* *Setup Example 2*

name,NF738 chno,10 dau,Neff  
desc,Body Balance Normal Force  
units,lbs  
euconv,lin  
lce(141.15448,0)  
filter,1  
cmplmt,-400  
cmpulmt,400  
dztype, wind  
pscorr(V738,5)

### \* *Equation Example 2*

$$\text{NF738} = ( ( \text{chan0010} * ( 5.0 / \text{V738} ) ) - \\ ( \text{chan0010}_{\text{woz}} * ( 5.0 / \text{V738}_{\text{woz}} ) ) ) * 141.15448$$

## POLY

### \* *Equation Definition*

$$\begin{aligned} \text{eu} = & \text{constant1} + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}}) * \text{constant2} ) \\ & + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}})^2 * \text{constant3} ) \\ & + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}})^3 * \text{constant4} ) \\ & + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}})^4 * \text{constant5} ) \\ & + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}})^5 * \text{constant6} ) \\ & + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}})^6 * \text{constant7} ) \\ & + ( (\text{chan#####} - \text{chan#####}_{\text{WOZ}})^7 * \text{constant8} ) \end{aligned}$$

### \* *Setup Example*

```
name,SROLL   chno,43   dau,Neff
desc,IRTS Shaft Roll
units,deg
euconv,coef
poly,3
lce(0.1847,-0.039,-0.2865,0.3239)
range,160
filter,1
cpllmt,-0.5
cplmt,0.5
dztype, no
```

### \* *Equation Example*

$$\begin{aligned} \text{SROLL} = & 0.1847 + ( \text{chan0043} * (-0.039) ) \\ & + ( ( \text{chan0043} )^2 * (-0.2865) ) \\ & + ( ( \text{chan0043} )^3 * 0.3239 ) \end{aligned}$$

## TYPE\_J

### \* *Equation Definition*

#### \* *type\_j denotes iron-constantan*

```
value = ( chan#### + jcn )  
* execute subfunction tcic(value, temp)  
eu = temp
```

### \* *Setup Example*

```
name,ESPTMP52   chno,65   dau,Neff  
desc,Temp of ESP52  
units,degf  
euconv,type_j  
range,10  
filter,1  
dztype, no  
jcn,0
```

### \* *Equation Example*

```
value = chan0065  
* execute subfunction tcic(value, temp)  
ESPTMP52 = temp
```

\* *note*            type\_k denotes chromel-alumel; execute subfunction **tcca**

\* *note*            type\_t denotes copper-constantan; execute subfunction **tccc**

## Tunnel Parameters

### Input Variables

ccust – customer dynamic pressure calibration constant (default = 0.0)  
dpicut – dpils/dpihs cutoff parameter (psf)  
dpihs – differential pressure of sidewall static pressure in the entrance cone  
referenced to ptot, used for high dynamic pressure (psf)  
dpils – differential pressure of sidewall static pressure in the entrance cone  
referenced to ptot, used for low dynamic pressure (psf);  
currently, value set to dpihs during engineering units' calculations  
kprcoef – dynamic pressure probe coefficient  
pa – ambient pressure (psf)  
pitot – test section dynamic pressure as measured by pitot tube (psf)  
ptot – settling chamber total pressure (psf)  
qcode – dynamic pressure computation code; constant  
qctn – dynamic pressure station; constant  
rjg - gas constant for air times gravitational constant  
ta – entrance cone ambient temperature (degF)  
tdew – dew point temperature (degF)  
wcode – test section configuration code for classical wall corrections; constant

### Output Variables

dpi – measured indicated difference between total and static pressure (psf)  
dpinf – dynamic pressure uncorrected for compressibility (psf)  
mach – free stream mach number with blockage corrections  
machu – uncorrected free stream mach number  
mu – absolute viscosity of air corrected for temperature (lbs/sec)  
pstat – test section static pressure with wall corrections (psf)  
pstatu – uncorrected test section static pressure (psf)  
pv – vapor pressure calculated from dew point (psf)  
q – tunnel dynamic pressure corrected for compressibility; wall corrections (psf)  
qu – uncorrected tunnel dynamic pressure with compressibility (psf)  
rho – air density corrected with blockage corrections (slugs/cf)  
rhoun – uncorrected air density (slugs/cf)  
rnft – test section reynolds number with blockage corrections (1/feet)  
rnftu – uncorrected test section reynolds number (1/feet)  
tr – ambient temperature (degR)  
vel – test section free stream velocity with wall corrections (ft/sec)  
velu – uncorrected test section free stream velocity (ft/sec)

\* *note*                      *Reference 14- by 22-Foot Subsonic Tunnel document entitled "Dynamic Pressure*  
\*                              *C alibration Corrections" for the current derivation of cprime.*

\* *note*                      *Cprime(dynamic pressure calibration coefficient) is calculated using equations*  
\*                              *determined by utilizing Check Standard Probe test results.*

\*                              *Cprime is not written to output data file*

**\* default values**

dpicut = 20.0  
rjg = 1716.2290  
kprcoef = 0.998  
pitot = 0.0

**\* tunnel total temperature** (degrees rankine)

tr = ta+459.67

**\* vapor pressure**

$$pv = 12.7654 * \exp(((9.72334 * tdew) - 311.147) / ((0.555556 * tdew) + 223.192))$$

**\* tunnel air density**

$$rho = (ptot - pv * 0.3789) / (rjg * tr)$$

**\* air viscosity**

$$\mu = 0.0002672 / (tr + 198.72) * (tr / 518.69) ** (1.5)$$

**\* QCODE Calculations**

```
if (qcode > 0) then
  dpi = 0.0
  dpinf = 0.0
  if (qcode > 1) then
    if (dpihs > dpicut) then
      dpi = dpihs
    else if (dpils > 0.0.and.dpils <= dpicut) then
      dpi = dpils
    endif
  endif
endif
```

```
if (qcode = 1.0) then
```

**\* Test Section PITOT Probe**

pitot = amax1(pitot,0.0)  
pstatu = ptot-pitot

```
else if ((qcode = 2.0) and (qcstn = 1.0)) then
```

**\* Closed Test Section, Boundary Layer Removal System Suction is Off**

dpinf = cprime\*kprcoef\*dpi  
pstatu = ptot-dpinf

else if ((qcode = 3.0) and (qcstn = 1.0)) then

**\* Closed Test Section, Boundary Layer Removal System Suction is On**

$dpinf = cprime * kprcoef * dpi$   
 $pstatu = ptot - dpinf$

else if ((qcode = 4.0) and (qcstn = 1.0)) then

**\* Open Test Section, Boundary Layer Removal System Suction is Off**

$dpinf = cprime * kprcoef * dpi$   
 $pstatu = ptot - dpinf$

else if (qcode = 5.0) then

**\* Open Test Section, Boundary Layer Removal System Suction is On**

$dpinf = cprime * kprcoef * dpi$   
 $pstatu = ptot - dpinf$

else if (qcode = 6.0) then

**\* Customer Assigned Calibration Constant**

$dpinf = ccust * dpi$   
 $pstatu = ptot - dpinf$

else if (qcode = 11.0) then

**\* Walls Up, Ceiling Down, Boundary Layer Removal System Suction is Off**

**\* *This calibration is out of date. Need new calibration for future test(s).***

$dpinf = cprime * kprcoef * dpi$   
 $pstatu = ptot - dpinf$

else if (qcode = 12.0) then

**\* Walls Up, Ceiling Down, Boundary Layer Removal System Suction is On**

**\* *This calibration is out of date. Need new calibration for future test(s).***

$dpinf = cprime * kprcoef * dpi$   
 $pstatu = ptot - dpinf$

else if (qcode = 13.0) then

**\* Walls Up, Ceiling Down, Boundary Layer Removal System Suction is Off,**

**\* *Vortex Vanes(Generators) are On***

$dpinf = cprime * kprcoef * dpi$   
 $pstatu = ptot - dpinf$

else

pstatu = ptot

endif

*\* note compressibility correction*  
*\* gamma = 1.4 (gas constant); -1.0 / gamma = -0.7143*

**\* density**

if (pstatu > 0.0) then  
  rhou = rhou\*(ptot/pstatu)\*\*(-0.7143)  
else  
  rhou = 0.0  
endif

**\* mach number**

if ((pstatu > 0.0) and ((ptot/pstatu) >= 1.0)) then  
  machu = sqrt(((ptot/pstatu)\*\*(2.0/7.0)-1.0)\*5.0)  
else  
  machu = 0.0  
endif

**\* dynamic pressure**

if (wcode = 0.0) then  
  xlamd = (ptot-pstatu)/ptot  
  qu = 3.5\*ptot\*((1.0-xlamd)\*\*(5.0/7.0)-1.0+xlamd)  
else  
  qu = 0.7\*pstatu\*machu\*machu  
endif  
if (qu < 0.001) then  
  qu = 0.0  
endif

**\* air velocity**

if (rhou > 0.0) then  
  velu = sqrt(abs(2.0\*qu/rhou))  
else  
  velu = 0.0  
endif

**\* reynolds number**

rnftu = rhou\*velu/mu

else

**\* values for qcode = 0.0**

```
dpi = 0.0  
dpinf = 0.0  
machu = 0.0  
pstatu = ptot  
qu = 0.0  
rhou = 0.0  
rnftu = 0.0  
velu = 0.0
```

```
endif
```

**\* initial values for corrected tunnel parameters**

```
mach = machu  
pstat = pstatu  
q = qu  
rho = rhou  
rnft = rnftu  
vel = velu
```



## Flowmeters

### Input Variables

flodp# – flowmeter differential pressure (psi)  
flop# – flowmeter inlet static pressure (psi)  
flotr# – flowmeter temperature (degR)  
ptot – settling chamber total pressure (psf)  
tr – ambient temperature (degR)

### Output Variables

flbeta# – flowmeter diameter ratio  
floasq# - cross-sectional area of throat (sqft)  
floc# - discharge coefficient  
flodi# – flowmeter inlet diameter (in)  
flodt# – flowmeter throat diameter (in)  
flov# - velocity of approach factor  
flomu# – flowmeter fluid viscosity (lbsec/ft)  
flopt# - flowmeter throat static pressure (psi)  
floptn# - normalized ambient pressure (psi)  
flor# - flowmeter pressure ratio  
florn# - flowmeter reynolds number  
flotf# - flowmeter temperature (degF)  
flottn# - normalized ambient temperature (degR)  
floy# - flowmeter expansion factor  
flsfmc# - flowmeter super compressibility factor  
wtflo# - mass flow rate (lbs/sec)  
wtflon# - normalized mass flow rate (lbs/sec)

\* *note*                *# is flowmeter number*  
\*                        *maximum number of flowmeters = 15*  
\*                        *the input and output variables aboved are per flowmeter*

\* *note*                *The source code routine, flowmeters.F, is used to perform the flowmeters' calculations.*

## Jet Exhaust Measurements

### Input Variables

fm1 – primary flow flowmeter frequency; air system 1 (Hz)  
fm2 – primary flow flowmeter frequency; air system 2 (Hz)  
fms – secondary flow flowmeter frequency (Hz)  
machu – uncorrected free stream mach number  
pbl1 – tertiary flow static pressure; probe 1 (psi)  
pbl2 – tertiary flow static pressure; probe 2 (psi)  
pbl3 – tertiary flow static pressure; probe3 (psi)  
pbl4 – tertiary flow static pressure; probe4 (psi)  
pch1 – plenum chamber total pressure; engine 1 (psi)  
pch2 – plenum chamber total pressure; engine 2 (psi)  
pch3 – plenum chamber total pressure; engine 3 (psi)  
pch4 – plenum chamber total pressure; engine 4 (psi)  
pfm1 – primary flow flowmeter pressure; air system 1 (psi)  
pfm2 – primary flow flowmeter pressure; air system 2 (psi)  
pfms – secondary flow flowmeter pressure; (psi)  
pstatu – uncorrected test section static pressure (psf)  
psv – venturi static pressure (psi)  
ps1 – primary jet static pressure; engine 1 (psi)  
ps2 – primary jet static pressure; engine 2 (psi)  
ps3 – primary jet static pressure; engine 3 (psi)  
ps4 – primary jet static pressure; engine 4 (psi)  
ptbl1 – tertiary flow total pressure; probe 1 (psi)  
ptbl2 – tertiary flow total pressure; probe 2 (psi)  
ptbl3 – tertiary flow total pressure; probe 3 (psi)  
ptbl4 – tertiary flow total pressure; probe 4 (psi)  
ptj1.1 – primary jet total pressure; engine 1, probe 1 (psi)  
ptj1.2 – primary jet total pressure; engine 1, probe 2 (psi)  
ptj1.3 – primary jet total pressure; engine 1, probe 3 (psi)  
ptj1.4 – primary jet total pressure; engine 1, probe 4 (psi)  
ptj1.5 – primary jet total pressure; engine 1, probe 5 (psi)  
ptj1.6 – primary jet total pressure; engine 1, probe 6 (psi)  
ptj1.7 – primary jet total pressure; engine 1, probe 7 (psi)  
ptj1.8 – primary jet total pressure; engine 1, probe 8 (psi)  
ptj1.9 – primary jet total pressure; engine 1, probe 9 (psi)  
ptj1.10 – primary jet total pressure; engine 1, probe 10 (psi)  
ptj1.11 – primary jet total pressure; engine 1, probe 11 (psi)  
ptj1.12 – primary jet total pressure; engine 2, probe 12 (psi)  
ptj2.1 – primary jet total pressure; engine 2, probe 1 (psi)  
ptj2.2 – primary jet total pressure; engine 2, probe 2 (psi)  
ptj2.3 – primary jet total pressure; engine 2, probe 3 (psi)  
ptj2.4 – primary jet total pressure; engine 2, probe 4 (psi)  
ptj2.5 – primary jet total pressure; engine 2, probe 5 (psi)  
ptj2.6 – primary jet total pressure; engine 2, probe 6 (psi)  
ptj2.7 – primary jet total pressure; engine 2, probe 7 (psi)  
ptj2.8 – primary jet total pressure; engine 2, probe 8 (psi)  
ptj2.9 – primary jet total pressure; engine 2, probe 9 (psi)

ptj2.10 – primary jet total pressure; engine 2, probe 10 (psi)  
 ptj2.11 – primary jet total pressure; engine 2, probe 11 (psi)  
 ptj2.12 – primary jet total pressure; engine 2, probe 12 (psi)  
 ptj3.1 – primary jet total pressure; engine 3, probe 1 (psi)  
 ptj3.2 – primary jet total pressure; engine 3, probe 2 (psi)  
 ptj3.3 – primary jet total pressure; engine 3, probe 3 (psi)  
 ptj3.4 – primary jet total pressure; engine 3, probe 4 (psi)  
 ptj3.5 – primary jet total pressure; engine 3, probe 5 (psi)  
 ptj3.6 – primary jet total pressure; engine 3, probe 6 (psi)  
 ptj3.7 – primary jet total pressure; engine 3, probe 7 (psi)  
 ptj3.8 – primary jet total pressure; engine 3, probe 8 (psi)  
 ptj3.9 – primary jet total pressure; engine 3, probe 9 (psi)  
 ptj3.10 – primary jet total pressure; engine 3, probe 10 (psi)  
 ptj3.11 – primary jet total pressure; engine 3, probe 11 (psi)  
 ptj3.12 – primary jet total pressure; engine 3, probe 12 (psi)  
 ptj4.1 – primary jet total pressure; engine 4, probe 1 (psi)  
 ptj4.2 – primary jet total pressure; engine 4, probe 2 (psi)  
 ptj4.3 – primary jet total pressure; engine 4, probe 3 (psi)  
 ptj4.4 – primary jet total pressure; engine 4, probe 4 (psi)  
 ptj4.5 – primary jet total pressure; engine 4, probe 5 (psi)  
 ptj4.6 – primary jet total pressure; engine 4, probe 6 (psi)  
 ptj4.7 – primary jet total pressure; engine 4, probe 7 (psi)  
 ptj4.8 – primary jet total pressure; engine 4, probe 8 (psi)  
 ptj4.9 – primary jet total pressure; engine 4, probe 9 (psi)  
 ptj4.10 – primary jet total pressure; engine 4, probe 10 (psi)  
 ptj4.11 – primary jet total pressure; engine 4, probe 11 (psi)  
 ptj4.12 – primary jet total pressure; engine 4, probe 12 (psi)  
 ptot – settling chamber total pressure (psf)  
 pts1 – secondary flow total pressure; probe 1 (psi)  
 pts2 – secondary flow total pressure; probe 2 (psi)  
 pts3 – secondary flow total pressure; probe 3 (psi)  
 pts4 – secondary flow total pressure; probe 4 (psi)  
 ptv – venturi total pressure (psi)  
 pven1.1 – multiple critical static pressure; air system1, upstream of  
                   venturi throat (psi)  
 pven1.2 – multiple critical static pressure; air system1, downstream of  
                   venturi throat (psi)  
 pven1.3 – multiple critical static pressure; air system1, upstream of  
                   venturi throat (psi)  
 pven1.4 – multiple critical static pressure; air system1, downstream of  
                   venturi throat (psi)  
 pven2.1 – multiple critical static pressure; air system 2, upstream of  
                   venturi throat (psi)  
 pven2.2 – multiple critical static pressure; air system 2, downstream of  
                   venturi throat (psi)  
 pven2.3 – multiple critical static pressure; air system 2, upstream of  
                   venturi throat (psi)  
 pven2.4 – multiple critical static pressure; air system 2, downstream of  
                   venturi throat (psi)  
 pvri1.1 – in-line(not mcv) venturi static pressure; air system 1, venturi 1 (psi)  
 pvri1.2 – in-line(not mcv) venturi static pressure; air system 1, venturi 2 (psi)

pvri1.3 – in-line(not mcv) venturi static pressure; air system 1, venturi 3 (psi)  
 pvri1.4 – in-line(not mcv) venturi static pressure; air system 1, venturi 4 (psi)  
 pvri2.1 – in-line(not mcv) venturi static pressure; air system 2, venturi 1 (psi)  
 pvri2.2 – in-line(not mcv) venturi static pressure; air system 2, venturi 2 (psi)  
 pvri2.3 – in-line(not mcv) venturi static pressure; air system 2, venturi 3 (psi)  
 pvri2.4 – in-line(not mcv) venturi static pressure; air system 2, venturi 4 (psi)  
 qu – uncorrected tunnel dynamic pressure with compressibility (psf)  
 tch1 – plenum chamber total temperature; engine 1 (degF)  
 tch2 – plenum chamber total temperature; engine 2 (degF)  
 tch3 – plenum chamber total temperature; engine 3 (degF)  
 tch4 – plenum chamber total temperature; engine 4 (degF)  
 tfm1 – primary flow flowmeter temperature; air system 1 (degF)  
 tfm2 – primary flow flowmeter temperature; air system 2 (degF)  
 tfms – secondary flow flowmeter temperature (degF)  
 ttbl – tertiary flow total temperature (degF)  
 ttj1.1 – primary jet total temperature; engine 1; probe 1 (degF)  
 ttj1.2 – primary jet total temperature; engine 1; probe 2 (degF)  
 ttj1.3 – primary jet total temperature; engine 1; probe 3 (degF)  
 ttj1.4 – primary jet total temperature; engine 1; probe 4 (degF)  
 ttj1.5 – primary jet total temperature; engine 1, probe 5 (degF)  
 ttj1.6 – primary jet total temperature; engine 1, probe 6 (degF)  
 ttj2.1 – primary jet total temperature, engine 2, probe 1 (degF)  
 ttj2.2 – primary jet total temperature; engine 2, probe 2 (degF)  
 ttj2.3 – primary jet total temperature; engine 2, probe 3 (degF)  
 ttj2.4 – primary jet total temperature; engine 2, probe 4 (degF)  
 ttj2.5 – primary jet total temperature; engine 2, probe 5 (degF)  
 ttj2.6 – primary jet total temperature; engine 2, probe 6 (degF)  
 ttj3.1 – primary jet total temperature; engine 3, probe 1 (degF)  
 ttj3.2 – primary jet total temperature; engine 3, probe 2 (degF)  
 ttj3.3 – primary jet total temperature; engine 3, probe 3 (degF)  
 ttj3.4 – primary jet total temperature; engine 3, probe 4 (degF)  
 ttj3.5 – primary jet total temperature; engine 3, probe 5 (degF)  
 ttj3.6 – primary jet total temperature; engine 3, probe 6 (degF)  
 ttj4.1 – primary jet total temperature; engine 4, probe 1 (degF)  
 ttj4.2 – primary jet total temperature; engine 4, probe 2 (degF)  
 ttj4.3 – primary jet total temperature; engine 4, probe 3 (degF)  
 ttj4.4 – primary jet total temperature; engine 4, probe 4 (degF)  
 ttj4.5 – primary jet total temperature; engine 4, probe 5 (degF)  
 ttj4.6 – primary jet total temperature; engine 4, probe 6 (degF)  
 ttsec – secondary flow total temperature; (degF)  
 ttv – tertiary flow venturi temperature (degF)  
 tv1.1 – venturi temperature; air system 1, venturi 1 (degF)  
 tv1.2 – venturi temperature; air system 1, venturi 2 (degF)  
 tv2.1 – venturi temperature; air system 2, venturi 1 (degF)  
 tv2.2 – venturi temperature; air system 2, venturi 2 (degF)  
 tvri1.1 – in-line(not mcv) venturi temperature; air system 1, venturi 1 (degF)  
 tvri1.2 – in-line(not mcv) venturi temperature; air system 1, venturi 2 (degF)  
 tvri1.3 – in-line(not mcv) venturi temperature; air system 1, venturi 3 (degF)  
 tvri1.4 – in-line(not mcv) venturi temperature; air system 1, venturi 4 (degF)  
 tvri2.1 – in-line(not mcv) venturi temperature; air system 2, venturi 1 (degF)  
 tvri2.2 – in-line(not mcv) venturi temperature; air system 2, venturi 2 (degF)

tvri2.3 – in-line(not mcv) venturi temperature; air system 2, venturi 3 (degF)  
tvri2.4 – in-line(not mcv) venturi temperature; air system 2, venturi 4 (degF)

## Output Variables

anlz1 – total throat area; air system 1  
anlz2 – total throat area; air system 2  
cfi1 – ideal thrust coefficient based on mass flow rate measured by flowmeter;  
air system 1  
cfi2 – ideal thrust coefficient based on mass flow rate measured by flowmeter;  
air system 2  
cfchr1 – ideal thrust coefficient based on mass flow rate computed from plenum  
chamber measurements; air system 1  
cfchr2 – ideal thrust coefficient based on mass flow rate computed from plenum  
chamber measurements; air system 2  
fi1 – ideal thrust of total primary exhaust system based on mass flow rate  
measured by flowmeter; air system 1 (lbs)  
fi2 – ideal thrust of total primary exhaust system based on mass flow rate  
measured by flowmeter; air system 2 (lbs)  
fia – average ideal thrust of total primary exhaust system (lbs)  
fichr1 – ideal thrust of total primary exhaust system based on mass flow rate  
computed from plenum chamber measurements; air system 1 (lbs)  
fichr2 – ideal thrust of total primary exhaust system based on mass flow rate  
computed from plenum chamber measurements; air system 2 (lbs)  
fieng1 – ideal thrust based on mass flow rate computed from individual  
plenum chamber measurements; engine 1 (lbs)  
fieng2 – ideal thrust based on mass flow rate computed from individual  
plenum chamber measurements; engine 2 (lbs)  
fieng3 – ideal thrust based on mass flow rate computed from individual  
plenum chamber measurements; engine 3 (lbs)  
fieng4 – ideal thrust based on mass flow rate computed from individual  
plenum chamber measurements; engine 4 (lbs)  
mblldot – tertiary flow mass flow rate (slugs/sec)  
mdot1 – primary flow mass flow rate measured by flowmeter;  
air system 1 (slugs/sec)  
mdot2 – primary flow mass flow rate measured by flowmeter;  
air system 2 (slugs/sec)  
mdota – average primary flow mass flow rate (slugs/sec)  
mdotch1 – primary flow mass flow rate computed from plenum chamber  
measurements; air system 1 (slugs/sec)  
mdotch 2 – primary flow mass flow rate computed from plenum chamber  
measurements; air system 2 (slugs/sec)  
mduct1 – mach number; engine 1  
mduct2 – mach number; engine 2  
mduct3 – mach number; engine 3  
mduct4 – mach number; engine 4  
msdot – secondary flow mass flow rate (slugs/sec)  
pblave – average tertiary flow static pressure (psi)  
pchoke – primary choked flow jet total pressure ratio  
pjet1 – primary jet pressure; air system 1 (psi)  
pjet2 – primary jet pressure; air system 2 (psi)

psec – average secondary flow static pressure (psi)  
 ptblav – average tertiary flow total pressure (psi)  
 ptb/pj - ratio of tertiary flow total pressure to primary jet total pressure  
 ptb/po – ratio of tertiary flow total pressure to free stream total pressure  
 pteng1 – average primary jet total pressure; engine 1 (psi)  
 pteng2 – average primary jet total pressure; engine 2 (psi)  
 pteng3 – average primary jet total pressure; engine 3 (psi)  
 pteng4 – average primary jet total pressure; engine 4 (psi)  
 ptengo1 – ratio of average primary jet total pressure in engine 1  
                   to tunnel static pressure  
 ptengo2 – ratio of average primary jet total pressure in engine 2  
                   to tunnel static pressure  
 ptengo3 – ratio of average primary jet total pressure in engine 3  
                   to tunnel static pressure  
 ptengo4 – ratio of average primary jet total pressure in engine 4  
                   to tunnel static pressure  
 ptj/po1 – primary jet total pressure ratio (all engines); air system 1  
 ptj/po2 – primary jet total pressure ratio (all engines); air system 2  
 ptj/poa – average primary jet total pressure ratio (all engines)  
 ptsec – average secondary flow total pressure (psi)  
 pts/po – ratio of secondary flow total pressure to free stream total pressure  
 pts/ptj – ratio of secondary flow total pressure to primary jet total pressure  
 pva1 – coefficient pv1; air system 1  
 pva2 – coefficient pv1; air system 2  
 tas1 – temperature; air system 1  
 tas2 – temperature; air system 2  
 thetase – secondary flow corrected mass flow ratio (slugs/sec)  
 thetbl – tertiary flow corrected mass flow rate (slugs/sec)  
 tteng1 – average primary jet total temperature; engine 1 (degF)  
 tteng2 – average primary jet total temperature; engine 2 (degF)  
 tteng3 – average primary jet total temperature; engine 3 (degF)  
 tteng4 – average primary jet total temperature; engine 4 (degF)  
 ttjav – average primary jet total temperature; all engines and air systems (degF)  
 ttjavgl – average primary jet total temperature; all engines,  
                   air system 1 (degF)  
 ttjavgl2 – average primary jet total temperature; all engines,  
                   air system 2 (degF)  
 tva1 – average venturi temperature; air system 1 (degF)  
 tva2 – average venturi temperature; air system 2 (degF)  
 vratio1 – ratio of multiple critical venturi static pressures; air system 1;  
                   should be less than 0.93  
 vratio2 – ratio of multiple critical venturi static pressures; air system 2;  
                   should be less than 0.93  
 wi1 – ideal weight flow rate; air system 1 (lbs/sec)  
 wi2 – ideal weight flow rate; air system 2 (lbs/sec)  
 wieng1 – ideal weight flow rate; engine 1 (lbs/sec)  
 wieng2 – ideal weight flow rate; engine 2 (lbs/sec)  
 wieng3 – ideal weight flow rate; engine 3 (lbs/sec)  
 wieng4 – ideal weight flow rate; engine 4 (lbs/sec)  
 wmcv1 – multiple critical venturi weight flow rate; air system 1 (lbs/sec)  
 wmcv2 – multiple critical venturi weight flow rate; air system 2 (lbs/sec)

wmcv/wi1 – ratio of multiple critical venturi weight flow rate to ideal weight flow rate; air system 1

wmcv/wi2 – ratio of multiple critical venturi weight flow rate to ideal weight flow rate; air system 2

wp1 – primary flow flowmeter weight flow rate; air system 1 (lbs/sec)

wp2 – primary flow flowmeter weight flow rate; air system 2 (lbs/sec)

wpbl – tertiary flow venturi weight flow rate (lbs/sec)

wpchr1 – total primary flow weight flow rate calculated from plenum chamber measurements; air system 1 (lbs/sec)

wpchr2 – total primary flow weight flow rate calculated from plenum chamber measurements; air system 2 (lbs/sec)

wpch/wi1 – total primary flow discharge coefficient computed from plenum chamber measurements; air system 1

wpch/wi2 – total primary flow discharge coefficient computed from plenum chamber measurements; air system 2

wpeng1 – primary flow weight flow rate computed from plenum chamber measurements; engine 1 (lbs/sec)

wpeng2 – primary flow weight flow rate computed from plenum chamber measurements; engine 2 (lbs/sec)

wpeng3 – primary flow weight flow rate computed from plenum chamber measurements; engine 3 (lbs/sec)

wpeng4 – primary flow weight flow rate computed from plenum chamber measurements; engine 4 (lbs/sec)

wpsec – secondary flow weight flow rate (lbs/sec)

wp/wi1 – primary flow discharge coefficient using flowmeter weight flow rate; air system 1

wp/wi2 – primary flow discharge coefficient using flowmeter weight flow rate; air system 2

wp/wie1 – discharge coefficient computed from plenum chamber measurements; engine 1

wp/wie2 – discharge coefficient computed from plenum chamber measurements; engine 2

wp/wie3 – discharge coefficient computed from plenum chamber measurements; engine 3

wp/wie4 – discharge coefficient computed from plenum chamber measurements; engine 4

wvri1.1 – in-line venturi weight flow rate; air system 1, venturi 1 (lbs/sec)

wvri1.2 – in-line venturi weight flow rate; air system 1, venturi 2 (lbs/sec)

wvri1.3 – in-line venturi weight flow rate; air system 1, venturi 3 (lbs/sec)

wvri1.4 – in-line venturi weight flow rate; air system 1, venturi 4 (lbs/sec)

wvri2.1 – in-line venturi weight flow rate; air system 2, venturi 1 (lbs/sec)

wvri2.2 – in-line venturi weight flow rate; air system 2, venturi 2 (lbs/sec)

wvri3.3 – in-line venturi weight flow rate; air system 2, venturi 3 (lbs/sec)

wvri4.4 – in-line venturi weight flow rate; air system 2, venturi 4 (lbs/sec)

\* *note*                      *The source code routine, modul2.F, is used to perform the jet exhaust*  
 \*                              *measurements' calculations.*



Refer to pages 14 thru 43 of reference 5 for a detailed explanation of the jet exhaust calculations.

Also, refer to reference 1 for information concerning the Multiple Critical Venturi System.



## **Balance Loads and Model Attitudes**

First, calculations are performed for initial loads and second order interactions due to initial loads. Next, corrections for first and second order balance interactions, high interactions/high model restraints, air line pressure, weight tares, method of attachment, and sting deflections are performed. Axis rotations follow these corrections.

Axis rotations include gravity axis to balance axis, gravity axis to model(body) axis, wind axis to gravity axis, and wind axis to model(body) axis. Angle calculations are performed for the balance and model(body) axes.

Next, calculations for the model height, balance components rotated and translated to the model(body) axis, applying estimates of Heyson's boundary interference, blockage and jet boundary corrections, Heyson's boundary(wall) interference, and base(cavity) pressures are performed. Finally, balance components and coefficients are calculated for the model, stability, wind, and reference axes.

Although only calculations for the balance one loads are explained, a maximum of four balances may be used. Unless noted, the calculations for balances two thru four are the same as the calculations for balance one. The variable names used in the calculations for each balance are named according to the balance number.

## Initial Loads

### Input Variables

phi0 – model roll angle at wind-off zero (deg)  
theta0 – model pitch angle at wind-off zero (deg)  
waf1 – axial force attitude load (lbs)  
wnf1 – axial force attitude load (lbs)  
wsf1 – side force attitude load (lbs)  
wxpm1 – pitching moment attitude load (in-lbs)  
wxy1 – yawing moment attitude load (in-lbs)  
wyr1 – rolling moment attitude load (in-lbs)  
wy1 – yawing moment attitude load (in-lbs)  
wzpm1 – pitching moment attitude load (in-lbs)  
wzr1 – rolling moment attitude load (in-lbs)

### Output Variables

af1.0 – axial force initial load (lbs)  
nf1.0 – normal force initial load (lbs)  
pm1.0 – pitching moment initial load (in-lbs)  
rm1.0 – rolling moment initial load (in-lbs)  
sf1.0 – side force initial load (lbs)  
ym1.0 – yawing moment initial load (in-lbs)

\* note  $dtor = 0.0174532925199$  {converts degrees to radians}

$$\begin{aligned}af1.0 &= waf1 * \sin(\theta_0 * dtor) \\sf1.0 &= wsf1 * \sin(\phi_0 * dtor) * \cos(\theta_0 * dtor) \\nf1.0 &= -wnf1 * \cos(\phi_0 * dtor) * \cos(\theta_0 * dtor) \\rm1.0 &= (wyr1 * \cos(\phi_0 * dtor) * \cos(\theta_0 * dtor)) + \\&\quad (wzr1 * \sin(\phi_0 * dtor) * \cos(\theta_0 * dtor)) \\pm1.0 &= (-wxpm1 * \cos(\phi_0 * dtor) * \cos(\theta_0 * dtor)) + \\&\quad (wzpm1 * \sin(\theta_0 * dtor)) \\ym1.0 &= (wxy1 * \sin(\phi_0 * dtor) * \cos(\theta_0 * dtor)) + \\&\quad (wy1 * \sin(\theta_0 * dtor))\end{aligned}$$

## Second Order Interactions Due To Initial Loads

### Input Variables

af1.0 – axial force initial load (lbs)  
nf1.0 – normal force initial load (lbs)  
pm1.0 – pitching moment initial load (in-lbs)  
rm1.0 – rolling moment initial load (in-lbs)  
sf1.0 – side force initial load (lbs)  
ym1.0 – yawing moment initial load (in-lbs)

### Output Variables

afez1 - axial force second order interactions due to initial loads (lbs)  
nfez1- normal force second order interactions due to initial loads (lbs)  
pmez1- pitching moment second order interactions due to initial loads (in-lbs)  
rmez1- rolling moment second order interactions due to initial loads (in-lbs)  
sfez1- side force second order interactions due to initial loads (lbs)  
ymez1- yawing moment second order interactions due to initial loads (in-lbs)

\* *note*                    *execute subfunction **ctrl** which computes the second order interactions*  
\*                            *due to initial loads.*

\* *note*                    *afez1, sfez1, nfez1, rmez1, pmez1, ymez1 are not written to output data file*

## First & Second Order Balance Interactions

### Input Variables

afez1 – axial force second order interactions due to initial loads(lbs)  
af1 – uncorrected axial force (lbs)  
af1.0 – axial force initial load (lbs)  
nfez1– normal force second order interactions due to initial loads(lbs)  
nf1 – uncorrected normal force (lbs)  
nf1.0 – normal force initial load (lbs)  
pmez1– pitching moment second order interactions due to initial loads(in-lbs)  
pm1 – uncorrected pitching moment (in-lbs)  
pm1.0 – pitching moment initial load (in-lbs)  
rmez1– rolling moment second order interactions due to initial loads(in-lbs)  
rm1 – uncorrected rolling moment (in-lbs)  
rm1.0 – rolling moment initial load (in-lbs)  
sfez1– side force second order interactions due to initial loads(lbs)  
sf1 – uncorrected side force (lbs)  
sf1.0 – side force initial load (lbs)  
ymez1– yawing moment second order interactions due to initial loads(in-lbs)  
ym1 – uncorrected yawing moment (in-lbs)  
ym1.0 – yawing moment initial load (in-lbs)

### Output Variables

af1.2 – axial force load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (lbs)  
nf1.2 – normal force load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (lbs)  
pm1.2 – pitching moment load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (in-lbs)  
rm1.2 – rolling moment load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (in-lbs)  
sf1.2 – side force load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (lbs)  
ym1.2 – yawing moment load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (in-lbs)

\* *note*                      *execute subfunction **cintr** which computes corrected delta loads for first*  
\*                              *and second order balance interactions.*

## High Interactions and High Model Restraints

The six balance loads are corrected for high interactions and high model restraints. A 6x6 balance interaction matrix is used for the interaction factors.

### Input Variables

af1.2 – axial force load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (lbs)  
b1aa1 – axial force(axial) interaction factor; constant; default value is 1.0  
b1na1 – axial force(normal) interaction factor; constant; default value is 0.0  
b1pa1 – axial force(pitch) interaction factor; constant; default value is 0.0  
b1ra1 – axial force(roll) interaction factor; constant; default value is 0.0  
b1sa1 – axial force(side) interaction factor; constant; default value is 0.0  
b1ya1 – axial force(yaw) interaction factor; constant; default value is 0.0  
b1an1 – normal force(axial) interaction factor; constant; default value is 0.0  
b1nn1 – normal force(normal) interaction factor; constant; default value is 1.0  
b1pn1 – normal force(pitch) interaction factor; constant; default value is 0.0  
b1rn1 – normal force(roll) interaction factor; constant; default value is 0.0  
b1sn1 – normal force(side) interaction factor; constant; default value is 0.0  
b1yn1 – normal force(yaw) interaction factor; constant; default value is 0.0  
b1ap1 – pitching moment(axial) interaction factor; constant; default value is 0.0  
b1np1 – pitching moment(normal) interaction factor; constant; default value is 0.0  
b1pp1 – pitching moment(pitch) interaction factor; constant; default value is 1.0  
b1rp1 – pitching moment(roll) interaction factor; constant; default value is 0.0  
b1sp1 – pitching moment(side) interaction factor; constant; default value is 0.0  
b1yp1 – pitching moment(yaw) interaction factor; constant; default value is 0.0  
b1ar1 – rolling moment(axial) interaction factor; constant; default value is 0.0  
b1nr1 – rolling moment(normal) interaction factor; constant; default value is 0.0  
b1pr1 – rolling moment(pitch) interaction factor; constant; default value is 0.0  
b1rr1 – rolling moment(roll) interaction factor; constant; default value is 1.0  
b1sr1 – rolling moment(side) interaction factor; constant; default value is 0.0  
b1yr1 – rolling moment(yaw) interaction factor; constant; default value is 0.0  
b1as1 – side force(axial) interaction factor; constant; default value is 0.0  
b1ns1 – side force(normal) interaction factor; constant; default value is 0.0  
b1ps1 – side force(pitch) interaction factor; constant; default value is 0.0  
b1rs1 – side force(roll) interaction factor; constant; default value is 0.0  
b1ss1 – side force(side) interaction factor; constant; default value is 1.0  
b1ys1 – side force(yaw) interaction factor; constant; default value is 0.0  
b1ay1 – yawing moment(axial) interaction factor; constant; default value is 0.0  
b1ny1 – yawing moment(normal) interaction factor; constant; default value is 0.0  
b1py1 – yawing moment(pitch) interaction factor; constant; default value is 0.0  
b1ry1 – yawing moment(roll) interaction factor; constant; default value is 0.0  
b1sy1 – yawing moment(side) interaction factor; constant; default value is 0.0  
b1yy1 – yawing moment(yaw) interaction factor; constant; default value is 1.0  
nf1.2 – normal force load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (lbs)  
pm1.2 – pitching moment load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (in-lbs)  
rm1.2 – rolling moment load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (in-lbs)  
sf1.2 – side force load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (lbs)  
ym1.2 – yawing moment load corrected for 1<sup>st</sup> & 2<sup>nd</sup> order balance interactions (in-lbs)

## Output Variables

af1.3 – axial force load corrected for high interactions and high model restraints (lbs)  
nf1.3 – normal force load corrected for high interactions and high model restraints (lbs)  
pm1.3 – pitching moment load corrected for high interactions and high model restraints (in-lbs)  
rm1.3 – rolling moment load corrected for high interactions and high model restraints (in-lbs)  
sf1.3 – side force load corrected for high interactions and high model restraints (lbs)  
ym1.3 – yawing moment load corrected for high interactions and high model restraints (in-lbs)

$$\text{af1.3} = (\text{af1.2} * \text{b1aa1}) + (\text{sf1.2} * \text{b1sa1}) + (\text{nf1.2} * \text{b1na1}) + (\text{rm1.2} * \text{b1ra1}) + (\text{pm1.2} * \text{b1pa1}) \\ + (\text{ym1.2} * \text{b1ya1})$$

$$\text{sf1.3} = (\text{af1.2} * \text{b1as1}) + (\text{sf1.2} * \text{b1ss1}) + (\text{nf1.2} * \text{b1ns1}) + (\text{rm1.2} * \text{b1rs1}) + (\text{pm1.2} * \text{b1ps1}) \\ + (\text{ym1.2} * \text{b1ys1})$$

$$\text{nf1.3} = (\text{af1.2} * \text{b1an1}) + (\text{sf1.2} * \text{b1sn1}) + (\text{nf1.2} * \text{b1nn1}) + (\text{rm1.2} * \text{b1rn1}) + (\text{pm1.2} * \text{b1pn1}) \\ + (\text{ym1.2} * \text{b1yn1})$$

$$\text{rm1.3} = (\text{af1.2} * \text{b1ar1}) + (\text{sf1.2} * \text{b1sr1}) + (\text{nf1.2} * \text{b1nr1}) + (\text{rm1.2} * \text{b1rr1}) + (\text{pm1.2} * \text{b1pr1}) \\ + (\text{ym1.2} * \text{b1yr1})$$

$$\text{pm1.3} = (\text{af1.2} * \text{b1ap1}) + (\text{sf1.2} * \text{b1sp1}) + (\text{nf1.2} * \text{b1np1}) + (\text{rm1.2} * \text{b1rp1}) + (\text{pm1.2} * \text{b1pp1}) \\ + (\text{ym1.2} * \text{b1yp1})$$

$$\text{ym1.3} = (\text{af1.2} * \text{b1ay1}) + (\text{sf1.2} * \text{b1sy1}) + (\text{nf1.2} * \text{b1ny1}) + (\text{rm1.2} * \text{b1ry1}) + (\text{pm1.2} * \text{b1py1}) \\ + (\text{ym1.2} * \text{b1yy1})$$

## Air Line Pressure Corrections

The six balance loads are corrected for air line pressure.

### Input Variables

af1.3 – axial force load corrected for high interactions and high model restraints (lbs)  
nf1.3 – normal force load corrected for high interactions and high model restraints (lbs)  
pca1.1 – axial force air line pressure coefficient 1; constant; default value is 0.0  
pca2.1 – axial force air line pressure coefficient 2; constant; default value is 0.0  
pca3.1 – axial force air line pressure coefficient 3; constant; default value is 0.0  
pcn1.1 – normal force air line pressure coefficient 1; constant; default value is 0.0  
pcn2.1 – normal force air line pressure coefficient 2; constant; default value is 0.0  
pcn3.1 – normal force air line pressure coefficient 3; constant; default value is 0.0  
pcp1.1 – pitching moment air line pressure coefficient 1; constant; default value is 0.0  
pcp2.1 – pitching moment air line pressure coefficient 2; constant; default value is 0.0  
pcp3.1 – pitching moment air line pressure coefficient 3; constant; default value is 0.0  
pcr1.1 – rolling moment air line pressure coefficient 1; constant; default value is 0.0  
pcr2.1 – rolling moment air line pressure coefficient 2; constant; default value is 0.0  
pcr3.1 – rolling moment air line pressure coefficient 3; constant; default value is 0.0  
pcs1.1 – side force air line pressure coefficient 1; constant; default value is 0.0  
pcs2.1 – side force air line pressure coefficient 2; constant; default value is 0.0  
pcs3.1 – side force air line pressure coefficient 3; constant; default value is 0.0  
pcy1.1 – yawing moment air line pressure coefficient 1; constant; default value is 0.0  
pcy2.1 – yawing moment air line pressure coefficient 2; constant; default value is 0.0  
pcy3.1 – yawing moment air line pressure coefficient 3; constant; default value is 0.0  
pm1.3 – pitching moment load corrected for high interactions and high model restraints (in-lbs)  
pst – air line pressure (psi)  
rm1.3 – rolling moment load corrected for high interactions and high model restraints (in-lbs)  
sf1.3 – side force load corrected for high interactions and high model restraints (lbs)  
ym1.3 – yawing moment load corrected for high interactions and high model restraints (in-lbs)

### Output Variables

af1.3 – axial force load corrected for high interactions, high model restraints and air line pressure (lbs)  
nf1.3 – normal force load corrected for high interactions, high model restraints and air line pressure (lbs)  
pm1.3 – pitching moment load corrected for high interactions, high model restraints, and air line pressure (in-lbs)  
rm1.3 – rolling moment load corrected for high interactions, high model restraints, and air line pressure (in-lbs)  
sf1.3 – side force load corrected for high interactions, high model restraints and air line pressure (lbs)  
ym1.3 – yawing moment load corrected for high interactions, high model restraints, and air line pressure (in-lbs)

$$\text{af1.3} = \text{af1.3} - ((\text{pst}*\text{pca1.1}) + (\text{pst}*\text{pst}*\text{pca2.1}) + (\text{pst}*\text{pst}*\text{pst}*\text{pca3.1}))$$

$$\text{sf1.3} = \text{sf1.3} - ((\text{pst}*\text{pcs1.1}) + (\text{pst}*\text{pst}*\text{pcs2.1}) + (\text{pst}*\text{pst}*\text{pst}*\text{pcs3.1}))$$

$$\text{nf1.3} = \text{nf1.3} - ((\text{pst}*\text{pcn1.1}) + (\text{pst}*\text{pst}*\text{pcn2.1}) + (\text{pst}*\text{pst}*\text{pst}*\text{pcn3.1}))$$

$$\text{rm1.3} = \text{rm1.3} - ((\text{pst}*\text{pcr1.1}) + (\text{pst}*\text{pst}*\text{pcr2.1}) + (\text{pst}*\text{pst}*\text{pst}*\text{pcr3.1}))$$

$$\text{pm1.3} = \text{pm1.3} - ((\text{pst}*\text{pcp1.1}) + (\text{pst}*\text{pst}*\text{pcp2.1}) + (\text{pst}*\text{pst}*\text{pst}*\text{pcp3.1}))$$

$$\text{ym1.3} = \text{ym1.3} - ((\text{pst}*\text{pcy1.1}) + (\text{pst}*\text{pst}*\text{pcy2.1}) + (\text{pst}*\text{pst}*\text{pst}*\text{pcy3.1}))$$



## Sting Deflections

### Input Variables

af1.0 - axial force initial load (lbs)  
af1.3 – axial force load corrected for high interactions, high model restraints  
and air line pressure (lbs)  
kdf1 – sting deflection corrections flag; constant  
nf1.0 - normal force initial load (lbs)  
nf1.3 – normal force load corrected for high interactions, high model restraints  
and air line pressure (lbs)  
phida1 – axial force roll deflection; constant  
phidn1 – normal force roll deflection; constant  
phidp1 – pitching moment roll deflection; constant  
phidr1 – rolling moment roll deflection; constant  
phids1 – side force roll deflection; constant  
phidy1 – yawing moment roll deflection; constant  
pm1.0 - pitching moment initial load (in-lbs)  
pm1.3 – pitching moment load corrected for high interactions, high model  
restraints, and air line pressure (in-lbs)  
psida1 – axial force yaw deflection; constant  
psidn1 – normal force yaw deflection; constant  
psidp1 – pitching moment yaw deflection; constant  
psidr1 – rolling moment yaw deflection; constant  
psids1 – side force yaw deflection; constant  
psidy1 – yawing moment yaw deflection; constant  
rm1.0 - rolling moment initial load (in-lbs)  
rm1.3 – rolling moment load corrected for high interactions, high model  
restraints, and air line pressure (in-lbs)  
sf1.0 - side force initial load (lbs)  
sf1.3 – side force load corrected for high interactions, high model restraints  
and air line pressure (lbs)  
theda1 – axial force pitch deflection; constant  
thedn1 – normal force pitch deflection; constant  
thedp1 – pitching moment pitch deflection; constant  
thedr1 – rolling moment pitch deflection; constant  
theds1 – side force pitch deflection; constant  
thedy1 – yawing moment pitch deflection; constant  
ym1.0 - yawing moment initial load (in-lbs)  
ym1.3 – yawing moment load corrected for high interactions, high model  
restraints, and air line pressure (in-lbs)

### Output Variables

phid – roll deflection angle (deg)  
psid – yaw deflection angle (deg)  
thetad – pitch deflection angle (deg)

\* *note*                      *The default value is 0.0 for phida1, phids1, phidn1, phidr1, phidp1,*  
 \*                              *phidy1, theda1, theds1, thedn1, thedr1, thedp1, thedy1, psida1, psids1,*  
 \*                              *psidn1, psidr1, psidp1, psidy1*

if ( kdf1 = -1 ) then

**\*no sting deflection corrections**

phid = 0.0  
 thetad = 0.0  
 psid = 0.0

else if ( kdf1 = 0 ) then

**\*sting deflection corrections using total loads**

phid = (phida1\*(af1.0+af1.3)) + (phids1\*(sf1.0+sf1.3)) +  
 (phidn1\*(nf1.0+nf1.3)) + (phidr1\*(rm1.0+rm1.3)) +  
 (phidp1\*(pm1.0+pm1.3)) + (phidy1\*(ym1.0+ym1.3))  
  
 thetad = (theda1\*(af1.0+af1.3)) + (theds1\*(sf1.0+sf1.3)) +  
 (thedn1\*(nf1.0+nf1.3)) + (thedr1\*(rm1.0+rm1.3)) +  
 (thedp1\*(pm1.0+pm1.3)) + (thedy1\*(ym1.0+ym1.3))  
  
 psid = (psida1\*(af1.0+af1.3)) + (psids1\*(sf1.0+sf1.3)) +  
 (psidn1\*(nf1.0+nf1.3)) + (psidr1\*(rm1.0+rm1.3)) +  
 (psidp1\*(pm1.0+pm1.3)) + (psidy1\*(ym1.0+ym1.3))

else if ( kdf1 = 1 ) then

**\*sting deflection corrections using delta loads**

phid = (phida1\*af1.3) + (phids1\*sf1.3) + (phidn1\*nf1.3) +  
 (phidr1\*rm1.3) + (phidp1\*pm1.3) + (phidy1\*ym1.3)  
  
 thetad = (theda1\*af1.3) + (theds1\*sf1.3) + thedn1\*nf1.3) +  
 (thedr1\*rm1.3) + (thedp1\*pm1.3) + (thedy1\*ym1.3)  
  
 psid = (psida1\*af1.3) + (psids1\*sf1.3) + (psidn1\*nf1.3) +  
 (psidr1\*rm1.3) + (psidp1\*pm1.3) + (psidy1\*ym1.3)

endif

## Weight Tares

### Input Variables

af1.3 – axial force load corrected for high interactions, high model restraints and air line pressure (lbs)  
nf1.3 – normal force load corrected for high interactions, high model restraints and air line pressure (lbs)  
phi – model roll angle (deg)  
phi0 – model roll angle at wind-off zero (deg)  
pm1.3 – pitching moment load corrected for high interactions, high model restraints, and air line pressure (in-lbs)  
rm1.3 – rolling moment load corrected for high interactions, high model restraints, and air line pressure (in-lbs)  
sf1.3 – side force load corrected for high interactions, high model restraints and air line pressure (lbs)  
theta – model pitch angle (deg)  
theta0 – model pitch angle at wind-off zero (deg)  
waf1 – axial force attitude load (lbs)  
wnf1 – axial force attitude load (lbs)  
wsf1 – side force attitude load (lbs)  
wxpm1 – pitching moment attitude load (in-lbs)  
wxym1 – yawing moment attitude load (in-lbs)  
wyrml – rolling moment attitude load (in-lbs)  
wyym1 – yawing moment attitude load (in-lbs)  
wzpm1 – pitching moment attitude load (in-lbs)  
wzrml – rolling moment attitude load (in-lbs)  
ym1.3 – yawing moment load corrected for high interactions, high model restraints, and air line pressure (in-lbs)

### Output Variables

aftare – axial force tare correction (lbs)  
af1.4 – axial force load corrected for weight tares (lbs)  
nftare – normal force tare correction (lbs)  
nf1.4 – normal force load corrected for weight tares (lbs)  
pmtare – pitching moment tare correction (in-lbs)  
pm1.4 – pitching moment load corrected for weight tares (in-lbs)  
rmtare – rolling moment tare correction (in-lbs)  
rm1.4 – rolling moment load corrected for weight tares (in-lbs)  
sftare – side force tare correction (lbs)  
sf1.4 – side force load corrected for weight tares (lbs)  
ymtare – yawing moment tare correction (in-lbs)  
ym1.4 – yawing moment load corrected for weight tares (in-lbs)

*\* note                    dtor = 0.0174532925199 {converts degrees to radians}*

```
aftare = waf1 * (sin(theta*dtor) - sin(theta0*dtor))
sftare = wsf1 * (cos(theta*dtor) * sin(phi*dtor)) -
          (cos(theta0*dtor) * sin(phi0*dtor))
nftare = -wnf1 * (cos(theta*dtor) * cos(phi*dtor)) -
          (cos(theta0*dtor) * cos(phi0*dtor))

if (waf1 = 0.0 & wsf1 = 0.0 & wnf1 = 0.0) then
  rmtare = 0.0
  pmtare = 0.0
  ymtare = 0.0
else
  rmtare = ((wzrm1/wsf1)*sftare) - ((wyrml/wnf1)*nftare)
  pmtare = ((wzpm1/waf1)*aftare) + ((wxpm1/wnf1)*nftare)
  ymtare = ((wxym1/wsf1)*sftare) + ((wyym1/waf1)*aftare)
endif

af1.4 = af1.3 - aftare
sf1.4 = sf1.3 - sftare
nf1.4 = nf1.3 - nftare
rm1.4 = rmf1.3 - rmtare
pm1.4 = pmf1.3 - pmtare
ym1.4 = ym1.3 - ymtare
```

## Method of Attachment

### Input Variables

af1.4 – axial force load corrected for weight tares (lbs)  
ksign1 – balance attachment; constant ( 1 = normal balance attachment,  
-1 = grounding balance by opposite end)  
nf1.4 – normal force load corrected for weight tares (lbs)  
pm1.4 – pitching moment load corrected for weight tares (in-lbs)  
rm1.4 – rolling moment load corrected for weight tares (in-lbs)  
sf1.4 – side force load corrected for weight tares (lbs)  
ym1.4 – yawing moment load corrected for weight tares (in-lbs)

### Output Variables

af1.5 – axial force load corrected for method of attachment (lbs)  
nf1.5 – normal force load corrected for method of attachment (lbs)  
pm1.5 – pitching moment load corrected for method of attachment (in-lbs)  
rm1.5 – rolling moment load corrected for method of attachment (in-lbs)  
sf1.5 – side force load corrected for method of attachment (lbs)  
ym1.5 – yawing moment load corrected for method of attachment (in-lbs)

$af1.5 = af1.4 * ksign1$   
 $sf1.5 = sf1.4 * ksign1$   
 $nf1.5 = nf1.4 * ksign1$   
 $rm1.5 = rm1.4 * ksign1$   
 $pm1.5 = pm1.4 * ksign1$   
 $ym1.5 = ym1.4 * ksign1$

## Angles' Calculations

Subfunction *euler* makes use of the angles' rotation flags and the 3 by 3 identity, yaw, pitch, and roll matrices to rotate(transform) angles from one axis to another axis. *Euler* is used to calculate the rotation matrices for the **gravity axis to balance axis**, **gravity axis to model(body) axis**, and **wind axis to gravity axis rotations**. These matrices are used to generate the angles' calculations.

### Identity matrix(3x3)

1.0	0.0	0.0
0.0	1.0	0.0
0.0	0.0	1.0

### Yaw matrix(3x3)

$\cos(\text{angle})$	$-\sin(\text{angle})$	0.0
$\sin(\text{angle})$	$\cos(\text{angle})$	0.0
0.0	0.0	1.0

### Pitch matrix(3x3)

$\cos(\text{angle})$	0.0	$-\sin(\text{angle})$
0.0	1.0	0.0
$\sin(\text{angle})$	0.0	$\cos(\text{angle})$

### Roll matrix(3x3)

1.0	0.0	0.0
0.0	$\cos(\text{angle})$	$-\sin(\text{angle})$
0.0	$\sin(\text{angle})$	$\cos(\text{angle})$

## Rotation of Angles from Gravity Axis to Balance Axis

### Input Variables

gbangles – nine-element array of angles (Euler input)  
gbflg – nine-element array of rotation flags (Euler input); one flag for each angle  
where values are [ -1 = yaw rotation, 0 = pitch rotation, 1 = roll rotation ]  
idmat – 3x3 identity array (Euler input)  
phid – deflection roll angle (deg)  
phik – knuckle roll angle (deg)  
phis – strut roll angle (deg)  
psid – deflection yaw angle (deg)  
psik – knuckle yaw angle (deg)  
psis – strut yaw angle (deg)  
thetad – deflection pitch angle (deg)  
thetak – knuckle pitch angle (deg)  
thetas – strut pitch angle (deg)

### Output Variables

gbmat – 3x3 gravity to balance axis array (Euler output)

*\* note                idmat and gbmat are double precision*

*\* note                idmat, gbangles, gbflg, gbmat are not written to output data file*

For a yaw-pitch-roll rotation, Let

```
gbangles(1) = psis
gbangles(2) = thetas
gbangles(3) = phis
gbangles(4) = psik
gbangles(5) = thetak
gbangles(6) = phik
gbangles(7) = psid
gbangles(8) = thetad
gbangles(9) = phid
gbflg(1) = -1
gbflg(2) = 0
gbflg(3) = 1
gbflg(4) = -1
gbflg(5) = 0
gbflg(6) = 1
gbflg(7) = -1
gbflg(8) = 0
gbflg(9) = 1
```

\* *note*                      *Input angles are in array **gbangles**, input matrix is **idmat**, and*  
 \*                              *rotation flags are in array **gbflg***

\**note*                      *Execute subfunction **euler** which performs angle rotation(s)*

\* *note*                      *Output matrix is **gbmat***

\* *note*                      *In special cases, up to **twelve knuckle angles** may be used;*  
 \*                              *the **other nine knuckle angles** are*

\*                              ***psij, thetaj, phij***

\*                              ***psip, thetap, phip***

\*                              ***psiv, thetav, phiv***



## Rotation of Angles from Gravity Axis to Model(Body) Axis

### Input Variables

gbmat – 3x3 gravity to balance axis array (Euler input)  
gmangles – three-element array of angles (Euler input)  
gmflg – three-element array of rotation flags(Euler input); one flag for each angle  
where values are [-1 = yaw rotation , 0 = pitch rotation, 1 = roll rotation ]  
phib – model(body) roll angle (deg)  
psib – model(body) yaw angle (deg)  
thetab – model(body) pitch angle (deg)

### Output Variables

gmmat – 3x3 gravity to model(body) axis array (Euler output)

*\* note                gbmata and gmmata are double precision*

*\* note                gmangles, gmflg, gbmata, and gmmata are not written to output data file*

For a yaw-pitch-roll rotation, Let

gmangles(1) = psib  
gmangles(2) = thetab  
gmangles(3) = phib  
gmflg(1) = -1  
gmflg(2) = 0  
gmflg(3) = 1

*\* note                Input angles are in array **gmangles**, input matrix is **gbmat**, and  
\*                        rotation flags are in array **gmflg***

*\*note                Execute subfunction **euler** which performs angle rotation(s)*

*\* note                Output matrix is **gmmat***

## Rotation of Angles from Wind Axis to Gravity Axis

### Input Variables

idmat - 3x3 identity array (Euler input)  
psiu – sideflow angle (deg)  
thetau – upflow angle (deg)  
wgangles - two-element array of angles (Euler input)  
wgflg - two-element array of rotation flags (Euler input); one flag for each angle  
where values are [0 = pitch rotation, -1 = yaw rotation]

### Output Variables

wgmat - 3x3 wind to gravity axis array (Euler output)

*\* note idmat and wgmat are double precision*

*\* note idmat, wgflg, wgmat are not written to output data file*

For a pitch-yaw rotation, Let

wgangles(1) = thetau  
wgangles(2) = psiu  
wgflg(1) = 0  
wgflg(2) = -1

*\* note Input angles are in array **wgangles**, input matrix is **idmat**, and  
\* rotation flags are in array **wgflg***

*\*note Execute subfunction **euler** which performs angle rotation(s)*

*\* note Output matrix is **wgmat***

## Rotation of Angles from Wind Axis to Model(Body) Axis

### Input Variables

gmmat - 3x3 gravity to model(body) axis array  
wgmata - 3x3 wind to gravity axis array

### Output Variables

wmmat - a 3x3 wind to model(body) axis array

\* *note*                *gmmat, wgmata, and wmmat are double precision*

\* *note*                *gmmat, wgmata, and wmmat are not written to output data file*

Let

gmmat =	gm11	gm12	gm13	gravity to model(body) axis matrix
	gm21	gm22	gm23	
	gm31	gm32	gm33	

and

wgmata =	wg11	wg12	wg13	wind to gravity axis matrix
	wg21	wg22	wg23	
	wg31	wg32	wg33	

then

wmmat =	wm11	wm12	wm13	wind to model(body) axis matrix
	wm21	wm22	wm23	
	wm31	wm32	wm33	

```
do k=1,3
  do j=1,3
    wm(j,k) = 0.0
    do i=1,3
      wm(j,k) = wm(j,k)+(gm(j,i)*wg(i,k))
    enddo
  enddo
enddo
```

## Balance Axis Angles

### Input Variables

gbmat - 3x3 gravity to balance axis array  
id – data identification flag

### Output Variables

phi – balance roll angle[-360 to +360 degrees] (deg)  
phi0 – balance roll angle[-360 to +360 degrees] at wind-off zero (deg)  
psi – balance yaw angle (deg)  
psi0 – balance yaw angle at wind-off zero (deg)  
theta – balance pitch angle (deg)  
theta0 – balance pitch angle at wind-off zero (deg)

- \* *note*                *rtod = 57.2957795131 {converts radians to degrees}*
- \* *note*                *gbmat is double precision*
- \* *note*                *gbmat, psi, and psi0 are not written to output data file*
- \* *note*                *datan2( value1, value2) = datan( value1 / value2)*  
\*                        *where datan2 is double precision arc tangent of two arguments*

### \* gravity to balance axis angles

Let

```
gbmat =      gb11  gb12  gb13
             gb21  gb22  gb23  (gravity to balance axis matrix)
             gb31  gb32  gb33
```

then

```
if ( gb12 = 0.0 & gb11 = 0.0 ) then
  psi = 0.0
else
  psi = datan2(-gb12, gb11) * rtod
endif
theta = dasin(-gb13) * rtod
if ( gb23 = 0.0 & gb33 = 0.0 ) then
  phi = 0.0
else
  phi = datan2(-gb23, gb33) * rtod
endif
```

*\* note                woz is wind-off zero flag number*

```
if ( id = woz ) then
  psi0 = psi
  theta0 = theta
  phi0 = phi
endif
```

## Model(Body) Axis Angles

### Input Variables

gmmat – 3x3 gravity to model(body) axis array  
wmmat – 3x3 wind to model(body)axis array

### Output Variables

alfunc – uncorrected model(body) angle of attack (deg)  
beta – model(body) sideslip angle (deg)  
modrol – model(body) roll angle (deg) [-180 to +180 degrees;  
used for airplane models]  
pitchgm1 – model(body) pitch angle  
rollgm1 – model(body) roll angle  
yawgm1 – model(body) yaw angle

\* *note*                    *rtod = 57.2957795131 {converts radians to degrees}*

\* *note*                    *gmmat and wmmat are double precision*

\* *note*                    *gmmat, wmmat, yawgm1, pitchgm1, and rollgm1*  
\*                         *are not written to output data file*

\* *note*                    *datan2( value1, value2) = datan( value1 / value2)*  
\*                         *where datan2 is double precision arc tangent of two arguments*

### \* gravity to model(body) axis angles

Let

	gm11 gm12 gm13	
gmmat =	gm21 gm22 gm23	gravity to model(body) axis matrix
	gm31 gm32 gm33	

then

```
if ( gm12 = 0.0 & gm11 = 0.0 ) then
  yawgm1 = 0.0
else
  yawgm1 = datan2(-gm12, gm11) * rtod
endif
pitchgm1 = dasin(-gm13) * rtod
```

```
if ( gm23 = 0.0 & gm33 = 0.0 ) then
  rollgm1 = 0.0
else
  rollgm1 = datan2(-gm23, gm33) * rtod
endif
```

**\* wind to model(body) axis angles**

Let

```
          wm11 wm12 wm13
wmmat =   wm21 wm22 wm23  wind to model(body) axis matrix
          wm31 wm32 wm33
```

then

```
beta = -dasin(wm21) * rtod
```

```
if ( wm31 = 0.0 & wm11 = 0.0 ) then
```

```
  alfunc = 0.0
```

```
else
```

```
  alfunc = datan2(wm31, wm11) * rtod
```

```
endif
```

```
if ( wm23 = 0.0 & wm22 = 0.0 ) then
```

```
  modrol = 0.0
```

```
else
```

```
  modrol = datan2(-wm23, wm22) * rtod
```

```
endif
```

## Model Height

### Input Variables

elev – cart elevation plus cart offset (inches)  
pitchm – mast pitch angle (deg)  
rlength – distance from (1) the center of the vertical mast to the model height reference point or  
(2) the center of the pitch rotation pivot to the model height reference point; constant (inches)  
scode – sting code; constant  
thetas – strut pitch angle (deg)  
vlength – vertical distance from the pivot center on the vertical strut to the model  
reference point; constant (inches)

### Output Variables

hgt – vertical distance from the test section floor to model height reference  
point (inches)

*\* note                    dtor = 0.0174532925199 {converts degrees to radians}*

if ( scode = 0.0 ) then

#### **\* no height calculation**

hgt = 0.0

else if (( scode = 1.0 ) or ( scode = 2.0 )) then

#### **\* height calculation for mast-mounted models or for alpha-beta sting**

hgt = 87.0+(elev-87.0)\*cos(pitchm\*dtor)+rlength\*sin(pitchm\*dtor)

else if ( scode = 3.0 ) then

#### **\* height calculation for vertical strut**

hgt = elev+rlength\*sin(thetas\*dtor)+vlength\*cos(thetas\*dtor)

endif



## Balance Components Rotated and Translated to Model Axis

### Input Variables

af1.5 – axial force load corrected for method of attachment (lbs)  
bcmangles - three-element array of angles (Euler input)  
bcmflg - three-element array of rotation flags (Euler input); one flag for each angle where values are [ -1 = yaw rotation, 0 = pitch rotation, 1 = roll rotation ]  
bcmmin - six-element array (Euler input)  
bspan1 – wing span; constant (ft)  
chord1 – wing aerodynamic chord; constant (ft)  
nf1.5 – normal force load corrected for method of attachment (lbs)  
phib – model(body) roll angle (deg)  
pm1.5 – pitching moment load corrected for method of attachment (in-lbs)  
psib – model(body) yaw angle (deg)  
q – tunnel dynamic pressure corrected for compressibility; wall corrections (psf)  
rm1.5 – rolling moment load corrected for method of attachment (in-lbs)  
sarea1 – wing area; constant (sqft)  
sf1.5 – side force load corrected for method of attachment (lbs)  
thetab – model(body) pitch angle (deg)  
xbar1 – moment transfer distance(x direction) measured in the model force axis system from the moment center to the desired moment center(positive in the direction of positive model thrust(axial), side and normal force (ft)  
ybar1 – moment transfer distance(y direction) measured in the model force axis system from the moment center to the desired moment center(positive in the direction of positive model thrust(axial), side and normal force (ft)  
ym1.5 – yawing moment load corrected for method of attachment (in-lbs)  
zbar1 – moment transfer distance(z direction) measured in the body force axis system from the moment center to the desired moment center(positive in the direction of positive model thrust(axial), side and normal force (ft)

### Output Variables

bcmout - six-element array (Euler output)  
fa1.1 - axial force rotated to the model axis (lbs)  
fa1.2 - axial force rotated and translated to the model axis (lbs)  
fn1.1 - normal force rotated to the model axis (lbs)  
fn1.2 - normal force rotated and translated to the model axis (lbs)  
fy1.1 - side force rotated to the model axis (lbs)  
fy1.2 - side force rotated and translated to the model axis (lbs)  
mx1.1 - rolling moment rotated to the model axis (in-lbs)  
mx1.2 - rolling moment rotated and translated to the model axis (in-lbs)  
my1.1 - pitching moment rotated to the model axis (in-lbs)  
my1.2 - pitching moment rotated and translated to the model axis (in-lbs)  
mz1.1 - yawing moment rotated to the model axis (in-lbs)  
mz1.2 - yawing moment rotated and translated to the model axis (in-lbs)

**\* forces and moments rotated to the model axis**

For a yaw-pitch-roll rotation, Let

```
bcmangles(1) = psib
bcmangles(2) = thetab
bcmangles(3) = phib
bcmflg(1) = -1
bcmflg(2) = 0
bcmflg(3) = 1
```

and

```
bcmin(1) = af1.5
bcmin(2) = sf1.5
bcmin(3) = nf1.5
bcmin(4) = -rm1.5
bcmin(5) = pm1.5
bcmin(6) = -ym1.5
```

*\* note                    execute subfunction **euler** which performs angle rotation(s)*

```
fa1.1 = bcmout(1)
fy1.1 = bcmout(2)
fn1.1 = bcmout(3)
mx1.1 = -bcmout(4)
my1.1 = bcmout(5)
mz1.1 = -bcmout(6)
```

**\* forces and moments rotated and translated to the model axis**

```
fa1.2 = fa1.1
fy1.2 = fy1.1
fn1.2 = fn1.1
mx1.2 = mx1.1 + ((fn1.1 * ybar1) - (fy1.1 * zbar1))
my1.2 = my1.1 - ((fn1.1 * xbar1) - (fa1.1 * zbar1))
mz1.2 = mz1.1 - ((fy1.1 * xbar1) - (fa1.1 * ybar1))
```

## Apply Estimates of Heyson's Corrections - Walls Up

### Input Variables

alfunc – uncorrected model(body) angle of attack (deg)  
dalup#.# - array of alpha correction coefficients; constants  
dolup# - array of drag over lift coefficients; constants  
dqup#.# - array of q correction coefficients; constants  
fa1.2 - axial force rotated and translated to the model axis (lbs)  
fn1.2 - normal force rotated and translated to the model axis (lbs)  
nbal – balance number; constant  
pa – ambient pressure (psf)  
qu – uncorrected tunnel dynamic pressure with compressibility (psf)  
sarea1 – wing area; constant (sqft)  
velu – uncorrected test section free stream velocity (ft/sec)  
wcode – test section configuration code for classical wall corrections; constant

### Output Variables

alpha – model(body) angle of attack with walls up or down corrections (deg)  
pstat – test section static pressure with walls up or down corrections (ft/sec)  
q – tunnel dynamic pressure corrected for compressibility; walls up or down corrections (psf)  
qcovrq – ratio of corrected dynamic pressure to uncorrected dynamic pressure  
vel – test section free stream velocity with walls up or down corrections (ft/sec)

*\* note                    dtor = 0.0174532925199 {converts degrees to radians}*

*\* note                    cls1u and cds1u are not written to output data file*

*\* note*

*\* array **dolup#** is            dolup1, dolup2, dolup3, dolup4, dolup5*

*\**

*\* array **dalup#.#** is        dalup1.1, dalup2.1, dalup3.1,*

*\*                                dalup1.2, dalup2.2, dalup3.2,*

*\*                                dalup1.3, dalup2.3, dalup3.3,*

*\*                                dalup1.4, dalup2.4, dalup3.4,*

*\*                                dalup1.5, dalup2.5, dalup3.5*

*\**

*\* array **dqup#.#** is        dqup1.1, dqup2.1, dqup3.1,*

*\*                                dqup1.2, dqup2.2, dqup3.2,*

*\*                                dqup1.3, dqup2.3, dqup3.3,*

*\*                                dqup1.4, dqup2.4, dqup3.4,*

*\*                                dqup1.5, dqup2.5, dqup3.5*

*\* note                    execute **walls up** calculations if **qu > 0.1 nbal = 1 wcode = 1***

**\* uncorrected stability axis lift coefficient**

$$cls1u = ((fn1.2 * \cos(alfunc * dtor)) - (fa1.2 * \sin(alfunc * dtor))) / (qu * sarea1)$$

**\* uncorrected stability axis drag coefficient**

$$cds1u = ((fa1.2 * \cos(alfunc * dtor)) + (fn1.2 * \sin(alfunc * dtor))) / (qu * sarea1)$$

\* *note*                    *execute subfunction **walcor** which computes corrected alpha and q*

**\* Tunnel parameters corrected for Q**

\* *note*                    **pstat** calculation below is being reviewed

$$vel = velu * \sqrt{q / qu}$$

$$pstat = pa - q$$

$$qcovrq = q / qu$$

## Apply Estimates of Heyson's Corrections - Walls Down

### Input Variables

alfunc – uncorrected model(body) angle of attack (deg)  
daldn#.# - array of alpha correction coefficients; constants  
doldn# - array of drag over lift coefficients; constants  
dqdn#.# - array of q correction coefficients; constants  
fa1.2 - axial force rotated and translated to the model axis (lbs)  
fn1.2 - normal force rotated and translated to the model axis (lbs)  
nbal – balance number; constant  
pa – ambient pressure (psf)  
qu – uncorrected tunnel dynamic pressure with compressibility (psf)  
sarea1 – wing area; constant (sqft)  
velu – uncorrected test section free stream velocity (ft/sec)  
wcode – test section configuration code for classical wall corrections; constant

### Output Variables

alpha – model(body) angle of attack with walls up or down corrections (deg)  
pstat – test section static pressure with walls up or down corrections (ft/sec)  
q – tunnel dynamic pressure corrected for compressibility; walls up or down corrections (psf)  
qcovrq – ratio of corrected dynamic pressure to uncorrected dynamic pressure  
vel – test section free stream velocity with walls up or down corrections (ft/sec)

\* note                     $dtor = 0.0174532925199$  {converts degrees to radians}

\* note                    *cls1u* and *cds1u* are not written to output data file

\* note

\* array **doldn#** is            *doldn1, doldn2, doldn3, doldn4, doldn5*

\*

\* array **daldn#.#** is        *daldn1.1, daldn2.1, daldn3.1,*

\*                                *daldn1.2, daldn2.2, daldn3.2,*

\*                                *daldn1.3, daldn2.3, daldn3.3,*

\*                                *daldn1.4, daldn2.4, daldn3.4,*

\*                                *daldn1.5, daldn2.5, daldn3.5*

\*

\* array **dqdn#.#** is        *dqdn1.1, dqdn2.1, dqdn3.1,*

\*                                *dqdn1.2, dqdn2.2, dqdn3.2,*

\*                                *dqdn1.3, dqdn2.3, dqdn3.3,*

\*                                *dqdn1.4, dqdn2.4, dqdn3.4,*

\*                                *dqdn1.5, dqdn2.5, dqdn3.5*

\* *note*                *execute walls down calculations if  $qu > 0.1$   $nbal = 1$   $wcode = 2$*

\* **uncorrected stability axis lift coefficient**

$$cls1u = ((fn1.2 * \cos(alfunc * dtor)) - (fa1.2 * \sin(alfunc * dtor))) / (qu * sarea1)$$

\* **uncorrected stability axis drag coefficient**

$$cds1u = ((fa1.2 * \cos(alfunc * dtor)) + (fn1.2 * \sin(alfunc * dtor))) / (qu * sarea1)$$

\* *note*                *execute subfunction **walcor** which computes corrected alpha and q*

\* **Tunnel parameters corrected for Q**

\* *note*                **pstat** calculation below is being reviewed

$$vel = velu * \sqrt{q / qu}$$

$$pstat = pa - q$$

$$qcovrq = q / qu$$

## Blockage and Jet Boundary Corrections

### Input Variables

alfunc – uncorrected model(body) angle of attack (deg)  
beta – model(body) sideslip angle (deg)  
bodyblok – solid-blockage velocity effect for a body of revolution; constant  
bspan1 – wing span; constant (ft)  
fa1.2 - axial force rotated and translated to the model axis (lbs)  
fn1.2 - normal force rotated and translated to the model axis (lbs)  
jbcorr2 – jet boundary angle of attack factor; constant  
machu – uncorrected free stream mach number  
pstatu – uncorrected test section static pressure (psf)  
qu – uncorrected tunnel dynamic pressure with compressibility (psf)  
rhou – uncorrected air density  
rnftu – uncorrected test section reynolds number  
sarea1 – wing area; constant (sqft)  
tsarea – test section area; constant  
velu – uncorrected test section free stream velocity  
wcode – test section configuration code for classical wall corrections; constant  
wingblok – solid-blockage velocity effect for a wing; constant

### Output Variables

alpha – model(body) angle of attack corrected for jet boundary (deg)  
delalp – jet boundary alpha correction  
mach – free stream mach number corrected for blockage  
pstat – test section static pressure; walls up or down or blockage corrections (psf)  
q – tunnel dynamic pressure corrected for compressibility;  
    walls up or walls down or blockage corrections (psf)  
qcovrq – ratio of corrected dynamic pressure to uncorrected dynamic pressure  
rho – air density corrected for blockage (slugscf)  
rnft – test section reynolds number corrected for blockage (1/feet)  
vel – test section free stream velocity; walls up or walls down or blockage corrections (ft/sec)

\* *note*            *pie, csaf, fds1u, cls1u, cd1u, acd, machu2, and bcf are*  
\*                    *not written to output data file*

\* *note*            *dtor = 0.0174532925199 {converts degrees to radians}*

if (wcode = 3) then

pie = 3.14159265

csaf = sarea1 / (tsarea \* 4.0)

**\* uncorrected stability axis drag force**

fds1u = (fa1.2 \* cos(alfunc \* dtor)) + (fn1.2 \* sin(alfunc \* dtor))

**\* uncorrected stability axis lift coefficient**

cls1u = ((fn1.2 \* cos(alfunc \* dtor)) - (fa1.2 \* sin(alfunc \* dtor))) / (qu \* sarea1)

**\* uncorrected wind axis drag coefficient**

cd1u = ((fds1u \* cos(beta \* dtor)) - (fy1.2 \* sin(beta \* dtor))) / (qu \* sarea1)

**\* Blockage calculations**

acd = cd1u - (cls1u \* cls1u \* sarea1) / (pie \* (bspan1 / 12.0)\*\*2)

machu2 = machu \* machu

**\* jbcorr4(blockage correction) is wingblok + bodyblok**

bcf = (wingblok + bodyblok) / (1.0 - machu2)\*\*1.5 + (1.0 + 0.4 \* machu2)  
\* acd \* csaf / (1.0 - machu2)

mach = machu \* (1.0 + (1.0 + 0.2 \* machu2) \* bcf)

pstat = pstatu \* (1.0 - 1.4 \* machu2 \* bcf)

q = qu \* (1.0 + (2.0 - machu2) \* bcf)

qcovrq = q / qu

rho = rhou \* (1.0 - machu2 \* bcf)

rnft = rnftu \* (1.0 + (1.0 - 0.7 \* machu2) \* bcf)

vel = velu \* (1.0 + bcf)

**\* Jet boundary angle of attack correction**

delalp = jbcorr2 \* cls1u

alpha = alfunc + delalp

endif



## Heyson's Boundary(Wall) Interference Functions

Harry Heyson wrote several documents which described calculating boundary(wall) interference factors for a variety of configurations. In reference 2, Heyson discussed sixteen software functions. Currenly, the 14- by 22-Foot Subsonic Tunnel's software utilizes function 2. Any of the other functions may be implemented upon request. The function number and the type of interference for a specific model are as follows.

<i><b>Function</b></i>	<i><b>Interference</b></i>
1	wind tunnel interference near a vanishingly small model
2	average wind tunnel interference over a swept wing
3	distribution od wind tunnel interference over the span of a swept wing
4	average wind tunnel interference over a tail behind a swept wing
5	average wind tunnel interference over a swept wing caused by the presence of lifting jets
6	distribution of wind tunnel interference over the span of a swept wing caused by the presence of lifting jets
7	average wind tunnel interference over a tail caused by the presence of lifting jets
8	average wind tunnel interference over a single rotor
9	distribution of wind tunnel interference over the lateral axis of a single rotor
10	distribution of wind tunnel interference over the longitudinal axis of a single rotor
11	average wind tunnel interference over a tail behind a single rotor
12	average wind tunnel interference over tandem rotors
13	average wind tunnel interference over unloaded rotor configuration
14	average wind tunnel interference over a tail behind an unloaded rotor configuration
15	average wind tunnel interference over side-by-side rotor configuration

16                    average wind tunnel interference over a tail behind a  
                         side-by-side rotor configuration

Refer to references 2, 3, and 4 for details concerning Heyson's boundary interference calculations.

## Heyson's Boundary(Wall) Interference Function 2 - Average Wind Tunnel Inteference Over a Swept Wing

### Input Variables

alfunc – uncorrected model(body) angle of attack (deg)  
 beta – model(body) sideslip angle (deg)  
 bspan1 – wing span; constant (ft)  
 fa1.2 - axial force rotated and translated to the model axis (lbs)  
 fn1.2 - normal force rotated and translated to the model axis (lbs)  
 gamma – ratio of tunnel width to height; constant  
 hannon – used in eta1 calculation; constant  
 hgt – height of the model height reference point above the test section floor (inches)  
 lambda – angle of sweep angle; constant  
 nbal – balance number; constant  
 q – tunnel dynamic pressure with compressibility; walls up or walls down or blockage corrections (psf)  
 rho – air density corrected for blockage (slugs/cf)  
 rlength – distance from (1) the center of the vertical mast to the model height reference point  
                   or (2) the center of the pitch rotation pivot to the model height reference point;  
                   constant (inches)  
 sarea1 – reference area; constant (sqft)  
 semispan – semispan model flag; constant  
 sigma – ratio of wing apn to the tunnel width; constant  
 tsarea – test section area; constant (sqft)  
 tsconf – test section configuration code for Heyson wall corrections; constant  
 vlength – vertical distance from the pivot center on the vertical strut to the model reference point;  
                   constant (inches)  
 wingar – wing aspect ratio; constant (ft)  
 wingload – wind load configuration; constant  
 zonecon – ratio of wind tunnel semi-height to height of model above tunnel floor; constant  
 zoneflg – zeta1 calculation flag; constant

### Output Variables

alfac – model(body) angle of attack with Heyson wall corrections (deg)  
 cdc – drag coefficient with Heyson wall corrections  
 clc – lift coefficient with Heyson wall corrections  
 dragc – drag corrected with Heyson wall corrections  
 liftc – lift corrected with Heyson wall corrections  
 lodc – lift over drag with Heyson wall corrections  
 qc – tunnel dynamic pressure corrected for compressibility; blockage & Heyson wall corrections (psf)  
 xeff – wake deflection angle (deg)

\* note                    *dtor = 0.0174532925199 {converts degrees to radians}*

\* note                    *if hannon = 0.0 rlength = 0.0 vlength = 0.0 then eta1 = 1.0*  
 \*                            *14x22-Foot Subsonic Tunnel is 21.75 feet wide and 14.5 feet high*  
 \*                            *gamma = 21.75 / 14.5 = 1.5*  
 \*                            *sigma = bspan1 / 21.75 where bspan1 is in feet*

```

*          wingar = (bpsan1 * bspan1) / sarea1  where bpsan1 is in feet and
*                                                    sarea1 is in square feet
*          tsarea = 21.75 * 14.5 = 315.375
*          bhtw = half the tunnel width (inches); not written to output data file

```

```

bhtw = 10.875 * 12.0
xeff = 0.0

```

```

if (nbal = 1.0 and tsconf > 0.0) then

```

```

    if (zoneflg = 1.0) then
        if (hgt > 0.0) then
            zeta1 = zonecon / hgt
        else
            zeta1 = zonecon
        endif
    else
        zeta1 = zonecon
    endif

```

```

    xwid = (hannon+(rlength*cos(alpha*dtor))-(vlength*sin(alpha*dtor)))
           * sin(beta*dtor)
    eta1 = (bhtw-xwid)/bhtw

```

```

    if (semispan = 0.0) then

```

**\* full wing span corrections**

```

        nforce = fn1.2
        aforce = fa1.2
        wrefarea = sarea1
        tsecarea = tsarea
        wingspan = bspan1

```

```

    else if (semispan = 1.0) then

```

**\* semi wing span corrections**

```

        nforce = fn1.2 * 2.0
        aforce = fa1.2 * 2.0
        wrefarea = sarea1 * 2.0
        tsecarea = tsarea * 2.0
        wingspan = bspan1 * 2.0

```

```

    endif

```

```

* note execute subfunction heyson as follows
*
*      call heyson(tsconf, wingload, zeta1, eta1, gamma, sigma, lambda,
*      nforce, aforce, qoc, rhoc, alfunc, wrefarea, wingar,
*      tsecarea, wingspan, liftc, dragc, clc, cdc, qc, alfac, xeff)

      if (semispan = 1.0) then
        liftc = liftc * 0.5
        dragc = dragc * 0.5
      endif

      lodc = clc / cdc

endif

```

## Base(Cavity) Pressures

### Input Variables

alpha - model angle of attack with jet boundary corrections (deg)  
arpba#.# – array of axial force base pressure areas; constant (sqft)  
arpbn#.# – array of normal force base pressure areas; constant (sqft)  
arpbp#.# – array of pitching moment base pressure moment arm\*areas; constant(in-sqft)  
arpbr#.# – array of rolling moment base pressure moment arm\*areas; constant (in-sqft)  
arpbs#.# – array of side force base pressure areas; constant (sqft)  
arpby#.# – array of yawing moment base pressure moment arm\*areas; constant (in-sqft)  
bspan1 – wing span; constant (ft)  
chord1 – wing aerodynamic chord; constant (ft)  
pbase# – array of base pressures (psf)  
pstat - tunnel static pressure with walls up/down or blockage corrections (psf)  
q – tunnel dynamic pressure with compressibility; walls up or walls down or blockage corrections (psf)  
sarea1 – wing area; constant (sqft)

### Output Variables

cabase1 - axial force base pressure tare coefficient calculated using axial force  
base pressure tare applied in final axial force calculation  
cdbase1 – drag base pressure tare coefficient  
cnbase1 – normal force base pressure tare coefficient  
cpbase# – array of base pressure coefficients  
cpmbase1 – pitching moment base pressure tare coefficient  
crmbase1 – rolling moment base pressure tare coefficient  
cybase1 – side force base pressure tare coefficient calculated using side force  
base pressure tare applied in final side force calculation  
cymbase1 – yawing moment base pressure tare coefficient  
dpbase# – array of differential base pressures (psf)  
fabase1 - axial force base pressure tare (lbs)  
fnbase1 - normal force base pressure tare (lbs)  
fybase1 - side force base pressure tare (lbs)  
pmbase1 - pitching moment base pressure tare (ft-lbs)  
rmbase1 - rolling moment base pressure tare (ft-lbs)  
ymbase1 - yawing moment base pressure tare (ft-lbs)

\* *note*                      *maximum number of base(cavity) pressures per balance is 25*  
\*                              *cavity pressures are calculated using base pressure names & equations*

#### \* **base(cavity) pressure areas (constants with default values of 0.0)**

arpba1.1	(axial force; base pressure 1, balance 1)
arpba2.1	(axial force; base pressure 2, balance 1)
arpba3.1	(axial force; base pressure 3, balance 1)
.	
.	
.	
arpba23.1	(axial force; base pressure 23, balance 1)

arpba24.1	(axial force; base pressure 24, balance 1)
arpba25.1	(axial force; base pressure 25, balance 1)
.	
.	
.	
arpby1.1	(yawing moment; base pressure 1, balance 1)
arpby2.1	(yawing moment; base pressure 2, balance 1)
arpby3.1	(yawing moment; base pressure 3, balance 1)
.	
.	
.	
arpby23.1	(yawing moment; base pressure 23, balance 1)
arpby24.1	(yawing moment; base pressure 24, balance 1)
arpby25.1	(yawing moment; base pressure 25, balance 1)

**\* differential base(cavity) pressures**

dpbase1 = pbase1-pstat	(base pressure 1)
dpbase2 = pbase2-pstat	(base pressure 2)
dpbase3 = pbase3-pstat	(base pressure 3)
.	
.	
.	
dpbase23 = pbase23-pstat	(base pressure 23)
dpbase24 = pbase24-pstat	(base pressure 24)
dpbase25 = pbase25-pstat	(base pressure 25)

**\* base(cavity) pressure coefficients**

cpbase1 = dpbase1/q	(base pressure 1)
cpbase2 = dpbase2/q	(base pressure 2)
cpbase3 = dpbase3/q	(base pressure 3)
.	
.	
.	
cpbase23 = dpbase23/q	(base pressure 23)
cpbase24 = dpbase24/q	(base pressure 24)
cpbase25 = dpbase25/q	(base pressure 25)

**\* base(cavity) pressure tares**

$$fabase1 = -((dpbase1*arpba1.1) + (dpbase2*arpba2.1) + (dpbase3*arpba3.1) + ....$$

$$+ (dpbase23*arpba23.1) + (dpbase24*arpba24.1) + (dpbase25*arpba25.1))$$

$$fybase1 = (dpbase1*arpbs1.1) + (dpbase2*arpbs2.1) + (dpbase3*arpbs3.1) + ....$$

$$+ (dpbase23*arpbs23.1) + (dpbase24*arpbs24.1) + (dpbase25*arpbs25.1)$$

$$fnbase1 = (dpbase1*arpbn1.1) + (dpbase2*arpbn2.1) + (dpbase3*arpbn3.1) + ....$$

$$+ (dpbase23*arpbn23.1) + (dpbase24*arpbn24.1) + (dpbase25*arpbn25.1)$$

$$\text{rmbase1} = (\text{dpbase1}*\text{arpbr1.1}) + (\text{dpbase2}*\text{arpbr2.1}) + (\text{dpbase3}*\text{arpbr3.1}) + \dots \\ + \text{dpbase23}*\text{arpbr23.1}) + (\text{dpbase24}*\text{arpbr24.1}) + (\text{dpbase25}*\text{arpbr25.1})$$

$$\text{pmbase1} = (\text{dpbase1}*\text{arpbp1.1}) + (\text{dpbase2}*\text{arpbp2.1}) + (\text{dpbase3}*\text{arpbp3.1}) + \dots \\ + \text{dpbase23}*\text{arpbp23.1}) + (\text{dpbase24}*\text{arpbp24.1}) + (\text{dpbase25}*\text{arpbp25.1})$$

$$\text{ymbase1} = (\text{dpbase1}*\text{arpby1.1}) + (\text{dpbase2}*\text{arpby2.1}) + (\text{dpbase3}*\text{arpby3.1}) + \dots \\ + \text{dpbase23}*\text{arpby23.1}) + (\text{dpbase24}*\text{arpby24.1}) + (\text{dpbase25}*\text{arpby25.1})$$

\* *note*  $\text{dtor} = 0.0174532925199$  {converts degrees to radians}

**\* base(cavity) pressure tare coefficients**

$$\begin{aligned} \text{cabase1} &= \text{fabase1}/(\text{q}*\text{sarea1}) \\ \text{cybase1} &= \text{fybase1}/(\text{q}*\text{sarea1}) \\ \text{cnbase1} &= \text{fnbase1}/(\text{q}*\text{sarea1}) \\ \text{crmbase1} &= \text{rmbase1}/(\text{q}*\text{sarea1}*\text{bspan1}) \\ \text{cpmbase1} &= \text{pmbase1}/(\text{q}*\text{sarea1}*\text{chord1}) \\ \text{cymbase1} &= \text{ymbase1}/(\text{q}*\text{sarea1}*\text{bspan1}) \end{aligned}$$

**\* base(cavity) pressure tare drag coefficient**

$$\text{cdbase1} = (\text{cabase1}*\cos(\alpha*\text{dtor})) + (\text{cnbase1}*\sin(\alpha*\text{dtor}))$$



## Model Axis Components and Coefficients

### Input Variables

bspan1 – wing span; constant (ft)  
chord1 – wing aerodynamic chord; constant (ft)  
fabase1 - axial force base pressure tare (lbs)  
fnbase1 - normal force base pressure tare (lbs)  
fybase1 - side force base pressure tare (lbs)  
pmbase1 - pitching moment base pressure tare (ft-lbs)  
q – tunnel dynamic pressure corrected for compressibility; walls up or walls down or  
blockage corrections (psf)  
rmbase1 - rolling moment base pressure tare (ft-lbs)  
sarea1 – wing area; constant (sqft)  
ymbase1 - yawing moment base pressure tare (ft-lbs)

### Output Variables

ca1 - model axis axial force coefficient corrected for base pressure tare  
cmx1 – model axis rolling moment coefficient corrected for base pressure tare  
cmy1 – model axis pitching moment coefficient corrected for base pressure tare  
cmz1 – model axis yawing moment coefficient corrected for base pressure tare  
cn1 – model axis normal force coefficient corrected for base pressure tare  
cy1 – model axis side force coefficient corrected for base pressure tare  
fa1 – model(body) axis axial force corrected for base pressure tare (lbs)  
fa1.2 - axial force rotated and translated to the model axis (lbs)  
fn1 – model(body) axis normal force corrected for base pressure tare (lbs)  
fn1.2 - normal force rotated and translated to the model axis (lbs)  
fy1 – model(body) axis side force corrected for base pressure tare (lbs)  
fy1.2 - side force rotated and translated to the model axis (lbs)  
mx1 – model(body) axis rolling moment corrected for base pressure tare (in-lbs)  
mx1.2 - rolling moment rotated and translated to the model axis (in-lbs)  
my1 – model(body) axis pitching moment corrected for base pressure tare (in-lbs)  
my1.2 - pitching moment rotated and translated to the model axis (in-lbs)  
mz1 – model(body) axis yawing moment corrected for delcm and base pressure tare (in-lbs)  
mz1.2 - yawing moment rotated and translated to the model axis (in-lbs)

### \* balance components

fa1 = fa1.2  
fy1 = fy1.2  
fn1 = fn1.2  
mx1 = mx1.2  
my1 = my1.2  
mz1 = mz1.2

**\* balance components & coefficients corrected for base pressure tares**

$$fa1 = fa1 - fabase1$$

$$fy1 = fy1 - fybase1$$

$$fn1 = fn1 - fnbase1$$

$$mx1 = mx1 - rmbase1$$

$$my1 = my1 - pmbase1$$

$$mz1 = mz1 - ymbase1$$

$$ca1 = fa1 / (q * sarea1)$$

$$cy1 = fy1 / (q * sarea1)$$

$$cn1 = fn1 / (q * sarea1)$$

$$cmx1 = mx1 / (q * sarea1 * bspan1)$$

$$cmy1 = my1 / (q * sarea1 * chord1)$$

$$cmz1 = mz1 / (q * sarea1 * bspan1)$$

## Stability Axis Components and Coefficients

### Input Variables

alpha – model angle of attack with jet boundary corrections (deg)  
bspan1 – wing span; constant (ft)  
chord1 – wing aerodynamic chord; constant (ft)  
fa1 – model(body) axis axial force corrected for base pressure tare (lbs)  
fn1 – model(body) axis normal force corrected for base pressure tare (lbs)  
fy1 – model(body) axis side force corrected for base pressure tare (lbs)  
mx1 – model(body) axis rolling moment corrected for base pressure tare (in-lbs)  
my1 – model(body) axis pitching moment corrected for base pressure tare (in-lbs)  
mz1 – model(body) axis yawing moment corrected for base pressure tare (in-lbs)  
q – tunnel dynamic pressure corrected for compressibility; walls up or walls down or  
blockage corrections (psf)  
sarea1 – wing area; constant (sqft)

### Output Variables

cds1 - stability axis drag coefficient corrected for base pressure tare  
clsqr1 – lift coefficient squared corrected for base pressure tare  
cls1 – stability axis lift coefficient corrected for base pressure tare  
cmxs1 – stability axis rolling moment coefficient corrected for base pressure tare  
cmys1 – stability axis pitching moment coefficient corrected for base pressure tare  
cmzs1 – stability axis yawing moment coefficient corrected for base pressure tare  
cys1 – model axis side force coefficient corrected for base pressure tare  
dell – jet boundary drag correction  
delp – jet boundary pitch correction  
fds1 – stability axis drag corrected for base pressure tare (lbs)  
fls1 – stability axis lift corrected for base pressure tare (lbs)  
fys1 – stability axis side force corrected for base pressure tare (lbs)  
ls/ds1 – lift-over-drag ratio corrected for base pressure tare  
mxs1 – stability axis rolling moment corrected for base pressure tare (in-lbs)  
mys1 – stability axis pitching moment corrected for base pressure tare (in-lbs)  
mzs1 – stability axis yawing moment corrected for base pressure tare (in-lbs)

\* *note*             $dtor = 0.0174532925199$  {converts degrees to radians}

### \* balance components & coefficients corrected for base pressure tares

$$fds1 = (fa1 * \cos(\alpha * dtor)) + (fn1 * \sin(\alpha * dtor))$$
$$fys1 = fy1$$
$$fls1 = (fn1 * \cos(\alpha * dtor)) - (fa1 * \sin(\alpha * dtor))$$
$$mxs1 = (mx1 * \cos(\alpha * dtor)) + (mz1 * \sin(\alpha * dtor))$$
$$mys1 = my1$$
$$mzs1 = (mz1 * \cos(\alpha * dtor)) - (mx1 * \sin(\alpha * dtor))$$

*\* jet boundary drag force correction*

```
dell = (jbcorr1 * fls1 * fls1) / (q * sarea1)  
fds1 = fds1 + dell
```

*\* jet boundary pitching moment correction*

```
delp = jbcorr3 * fls1 * chord1  
mys1 = mys1 - delp
```

```
cds1 = fds1 / (q * sarea1)  
cys1 = fys1 / (q * sarea1)  
cls1 = fls1 / (q * sarea1)  
cmxs1 = mxs1 / (q * sarea1 * bspan1)  
cmys1 = mys1 / (q * sarea1 * chord1)  
cmzs1 = mzs1 / (q * sarea1 * bspan1)
```

```
ls/ds1 = cls1 / cds1  
clsqr1 = cls1 * cls1
```

## Wind Axis Components and Coefficients

### Input Variables

beta – model sideslip angle (deg)  
bspan1 – wing span; constant (ft)  
chord1 – wing aerodynamic chord; constant (ft)  
fds1 – stability axis drag corrected for base pressure tare (lbs)  
fls1 – stability axis lift corrected for base pressure tare (lbs)  
fys1 – stability axis side force corrected for base pressure tare (lbs)  
mxs1 – stability axis rolling moment corrected for base pressure tare (in-lbs)  
mys1 – stability axis pitching moment corrected for base pressure tare (in-lbs)  
mzs1 – stability axis yawing moment corrected for base pressure tare (in-lbs)  
q – tunnel dynamic pressure corrected for compressibility; walls up or walls down or blockage corrections (psf)  
sarea1 – wing area; constant (sqft)

### Output Variables

cc1 – wind axis crosswind coefficient corrected for base pressure tare  
cd1 – wind axis drag coefficient corrected for base pressure tare  
cl1 – wind axis lift coefficient corrected for base pressure tare  
cmxw1 – wind axis rolling moment coefficient corrected for base pressure tare  
cmyw1 – wind axis pitching moment coefficient corrected for base pressure tare  
cmzw1 – wind axis yawing moment coefficient corrected for base pressure tare  
fc1 – wind axis crosswind corrected for base pressure tare (lbs)  
fd1 – wind axis drag corrected for base pressure tare (lbs)  
fl1 – wind axis lift corrected for base pressure tare (lbs)  
ld1 – lift-over-drag ratio corrected for base pressure tare  
mxw1 – wind axis rolling moment corrected for base pressure tare (in-lbs)  
myw1 – wind axis pitching moment corrected for base pressure tare (in-lbs)  
mzw1 – wind axis yawing moment corrected for base pressure tare (in-lbs)

\* note  $dtor = 0.0174532925199$  {converts degrees to radians}

### \* balance components & coefficients corrected for base pressure tares

$fd1 = (fds1 * \cos(\text{beta} * dtor)) - (fys1 * \sin(\text{beta} * dtor))$   
 $fc1 = (fys1 * \cos(\text{beta} * dtor)) + (fds1 * \sin(\text{beta} * dtor))$   
 $fl1 = fls1$   
 $mxw1 = (mxs1 * \cos(\text{beta} * dtor)) + (mys1 * \sin(\text{beta} * dtor))$   
 $myw1 = (mys1 * \cos(\text{beta} * dtor)) - (mxs1 * \sin(\text{beta} * dtor))$   
 $mzw1 = mzs1$

```
cd1 = fd1 / (q * sarea1)
cc1 = fc1 / (q * sarea1)
cl1 = fl1 / (q * sarea1)
cmxw1 = mxw1 / (q * sarea1 * bspan1)
cmyw1 = myw1 / (q * sarea1 * chord1)
cmzw1 = mzw1 / (q * sarea1 * bspan1)

ld1 = cl1 / cd1
```

## Reference Axis Components and Coefficients

### Input Variables

bspan1 – wing span; constant (ft)  
chord1 – wing aerodynamic chord; constant (ft)  
fa1 – model(body) axis axial force corrected for base pressure tare (lbs)  
fn1 – model(body) axis normal force corrected for base pressure tare (lbs)  
fy1 – model(body) axis side force corrected for base pressure tare (lbs)  
mx1 – model(body) axis rolling moment corrected for base pressure tare (in-lbs)  
my1 – model(body) axis pitching moment corrected for base pressure tare (in-lbs)  
mz1 – model(body) axis yawing moment corrected for base pressure tare (in-lbs)  
phir1 – reference axis roll angle (deg)  
psir1 – reference axis yaw angle (deg)  
q – tunnel dynamic pressure corrected for compressibility; walls up or walls down or blockage corrections (psf)  
refangles - three-element array of angles (Euler input)  
refflg - three-element array of rotation flags (Euler input);  
          one flag for each angle where values are [ -1 = yaw rotation, 0 = pitch rotation, 1 = roll rotation ]  
refin - six-element array (Euler input)  
sarea1 – wing area; constant (sqft)  
thetar1 – reference axis pitch angle (deg)  
xref1 – moment transfer distance(x direction) measured in the model force axis system from the moment center to the desired moment center(positive in the direction of positive model thrust(axial), side and normal force (ft)  
yref1 – moment transfer distance(y direction) measured in the model force axis system from the moment center to the desired moment center(positive in the direction of positive model thrust(axial), side and normal force (ft)  
zref1 – moment transfer distance(z direction) measured in the body force axis system from the moment center to the desired moment center(positive in the direction of positive model thrust(axial), side and normal force (ft)

### Output Variables

faref1 – model(body) axis axial force rotated and translated to an arbitrary reference axis (lbs)  
farefr1 – model(body) axis axial force rotated to an arbitrary reference axis (lbs)  
fnref1 – model (body) axis normal force rotated and translated to an arbitrary reference axis (lbs)  
fnrefr1 – model (body) axis normal force rotated to an arbitrary reference axis (lbs)  
fyref1 – model (body) axis side force rotated and translated to an arbitrary reference axis (lbs)  
fyrefr1 – model (body) axis side force rotated to an arbitrary reference axis (lbs)  
mxref1 – model (body) axis rolling moment rotated and translated to an arbitrary reference axis (in-lbs)  
mxrefr1 – model (body) axis rolling moment rotated to an arbitrary reference axis (in-lbs)  
myref1 – model (body) axis pitching moment rotated and translated to an arbitrary reference axis (in-lbs)  
myrefr1 – model (body) axis pitching moment rotated to an arbitrary reference axis (in-lbs)  
mzref1 – model (body) axis yawing moment rotated and translated to an arbitrary reference axis (in-lbs)  
mzrefr1 – model (body) axis yawing moment rotated to an arbitrary reference axis (in-lbs)  
refout - six-element array (Euler output)

**\* forces and moments rotated to the model axis**

For a yaw-pitch-roll rotation, Let

```
refangles(1) = psir1  
refangles(2) = thetar1  
refangles(3) = phir1  
refflg(1) = -1  
refflg(2) = 0  
refflg(3) = 1
```

and

```
refin(1) = fa1  
refin(2) = fy1  
refin(3) = fn1  
refin(4) = -mx1  
refin(5) = my1  
refin(6) = -mz1
```

*\* note                    execute subfunction **euler** which performs angle rotation(s)*

**\* model(body) axis components rotated to an arbitrary reference axis**

```
farefr1 = refout(1)  
fyrefr1 = refout(2)  
fnrefr1 = refout(3)  
mxrefr1 = -refout(4)  
myrefr1 = refout(5)  
mzrefr1 = -refout(6)
```

**\* model(body) axis components and coefficients rotated and translated to  
\* an arbitrary reference axis**

```
faref1 = farefr1  
fyref1 = fyrefr1  
fnref1 = fnrefr1  
mxref1 = mxrefr1 + (fnrefr1 * yref1) - (fyrefr1 * zref1)  
myref1 = myrefr1 - (fnrefr1 * xref1) - (farefr1 * zref1)  
mzref1 = mzrefr1 - (fyrefr1 * xref1) - (farefr1 * yref1)  
  
caref1 = faref1 / (q * sareal)  
cyref1 = fyref1 / (q * sareal)  
cnref1 = fnref1 / (q * sareal)  
cmxref1 = mxref1 / (q * sareal * bspan1)  
cmymref1 = myref1 / (q * sareal * chord1)  
cmzref1 = mzref1 / (q * sareal * bspan1)
```



## Model and Wall Pressures

### Input Variables

dpat – difference between the settling chamber total pressure and the ambient pressure “ptot - pa” (psf)  
dpinf – dynamic pressure uncorrected for compressibility (psf)  
dprr – WICS set pressure (psf)  
p# – array of esp pressures (psf)  
q – tunnel dynamic pressure corrected for compressibility; wall corrections (psf)  
qu – uncorrected tunnel dynamic pressure with compressibility (psf)  
wsp# – array of WICS esp pressures (psf)

### Output Variables

cpp# – array of pressure coefficients  
wpp# – array of WICS pressure coefficients

\* *note*                    *maximum number of esp modules = 16*  
\*                            *maximum number of pressures per esp module = 64*

\* *note*                    *qcalc is not written to output data file*

#### \* **pressure coefficients**

```
if (q.eq.0.0) then
  qcalc = 1.0
else
  qcalc = q
endif

cpp101 = (p101-dpat+dpinf)/qcalc      (module 1, port 1)
cpp102 = (p102-dpat+dpinf)/qcalc      (module 1, port 2)
cpp103 = (p103-dpat+dpinf)/qcalc      (module 1, port 3)
.
.
.
cpp162 = (p162-dpat+dpinf)/qcalc      (module 1, port 62)
cpp163 = (p163-dpat+dpinf)/qcalc      (module 1, port 63)
cpp164 = (p164-dpat+dpinf)/qcalc      (module 1, port 64)
.
.
.
cpp1601 = (p1601-dpat+dpinf)/qcalc    (module 16, port 1)
cpp1602 = (p1602-dpat+dpinf)/qcalc    (module 16, port 2)
cpp1603 = (p1603-dpat+dpinf)/qcalc    (module 16, port 3)
.
.
.
cpp1662 = (p1662-dpat+dpinf)/qcalc    (module 16, port 62)
cpp1663 = (p1663-dpat+dpinf)/qcalc    (module 16, port 63)
```

$cpp1664 = (p1664 - dpat + dpinf) / qcalc$  (module 16, port 64)

**\* Wall Interference Correction System pressures**

```
if (qu.eq.0.0) then
  qcalc = 1.0
else
  qcalc = qu
endif
```

**\* South Wall Pressures**

$wpp5001 = (wsp5001 + dpinf - dprr) / qcalc$	(module 50, port 1)
$wpp5002 = (wsp5002 + dpinf - dprr) / qcalc$	(module 50, port 2)
$wpp5003 = (wsp5003 + dpinf - dprr) / qcalc$	(module 50, port 3)
.	
.	
.	
$wpp5062 = (wsp5062 + dpinf - dprr) / qcalc$	(module 50, port 62)
$wpp5063 = (wsp5063 + dpinf - dprr) / qcalc$	(module 50, port 63)
$wpp5064 = (wsp5064 + dpinf - dprr) / qcalc$	(module 50, port 64)
$wpp5101 = (wsp5101 + dpinf - dprr) / qcalc$	(module 51, port 1)
$wpp5102 = (wsp5102 + dpinf - dprr) / qcalc$	(module 51, port 2)
$wpp5103 = (wsp5103 + dpinf - dprr) / qcalc$	(module 51, port 3)
.	
.	
.	
$wpp5162 = (wsp5162 + dpinf - dprr) / qcalc$	(module 51, port 62)
$wpp5163 = (wsp5163 + dpinf - dprr) / qcalc$	(module 51, port 63)
$wpp5164 = (wsp5164 + dpinf - dprr) / qcalc$	(module 51, port 64)

**\* Ceiling Pressures**

$wpp5201 = (wsp5201 + dpinf - dprr) / qcalc$	(module 52, port 1)
$wpp5202 = (wsp5202 + dpinf - dprr) / qcalc$	(module 52, port 2)
$wpp5203 = (wsp5203 + dpinf - dprr) / qcalc$	(module 52, port 3)
.	
.	
.	
$wpp5262 = (wsp5262 + dpinf - dprr) / qcalc$	(module 52, port 62)
$wpp5263 = (wsp5263 + dpinf - dprr) / qcalc$	(module 52, port 63)
$wpp5264 = (wsp5264 + dpinf - dprr) / qcalc$	(module 52, port 64)
$wpp5301 = (wsp5301 + dpinf - dprr) / qcalc$	(module 53, port 1)
$wpp5302 = (wsp5302 + dpinf - dprr) / qcalc$	(module 53, port 2)
$wpp5303 = (wsp5303 + dpinf - dprr) / qcalc$	(module 53, port 3)

.  
 .  
 .  
 $wpp5362 = (wsp5362 + dpinf - dprr) / qcalc$  (module 53, port 62)  
 $wpp5363 = (wsp5363 + dpinf - dprr) / qcalc$  (module 53, port 63)  
 $wpp5364 = (wsp5364 + dpinf - dprr) / qcalc$  (module 53, port 64)

\* **North Wall Pressures**

$wpp5401 = (wsp5401 + dpinf - dprr) / qcalc$  (module 54, port 1)  
 $wpp5402 = (wsp5402 + dpinf - dprr) / qcalc$  (module 54, port 2)  
 $wpp5403 = (wsp5403 + dpinf - dprr) / qcalc$  (module 54, port 3)  
 .  
 .  
 .  
 $wpp5462 = (wsp5462 + dpinf - dprr) / qcalc$  (module 54, port 62)  
 $wpp5463 = (wsp5463 + dpinf - dprr) / qcalc$  (module 54, port 63)  
 $wpp5464 = (wsp5464 + dpinf - dprr) / qcalc$  (module 54, port 64)  
  
 $wpp5501 = (wsp5501 + dpinf - dprr) / qcalc$  (module 55, port 1)  
 $wpp5502 = (wsp5502 + dpinf - dprr) / qcalc$  (module 55, port 2)  
 $wpp5503 = (wsp5503 + dpinf - dprr) / qcalc$  (module 55, port 3)  
 .  
 .  
 .  
 $wpp5562 = (wsp5562 + dpinf - dprr) / qcalc$  (module 55, port 62)  
 $wpp5563 = (wsp5563 + dpinf - dprr) / qcalc$  (module 55, port 63)  
 $wpp5564 = (wsp5564 + dpinf - dprr) / qcalc$  (module 55, port 64)

\* **South Wall Centerline Pressures**

$wpp5701 = (wsp5701 + dpinf - dprr) / qcalc$  (module 57, port 1)  
 $wpp5702 = (wsp5702 + dpinf - dprr) / qcalc$  (module 57, port 2)  
 $wpp5703 = (wsp5703 + dpinf - dprr) / qcalc$  (module 57, port 3)  
 .  
 .  
 .  
 $wpp5730 = (wsp5730 + dpinf - dprr) / qcalc$  (module 57, port 30)  
 $wpp5731 = (wsp5731 + dpinf - dprr) / qcalc$  (module 57, port 31)  
 $wpp5732 = (wsp5732 + dpinf - dprr) / qcalc$  (module 57, port 32)

\* **Ceiling Centerline Pressures**

$wpp5801 = (wsp5801 + dpinf - dprr) / qcalc$  (module 58, port 1)  
 $wpp5802 = (wsp5802 + dpinf - dprr) / qcalc$  (module 58, port 2)  
 $wpp5803 = (wsp5803 + dpinf - dprr) / qcalc$  (module 58, port 3)  
 .

.  
 .  
 $wpp5830 = (wsp5830 + dpinf - dp_{prt}) / q_{calc}$  (module 58, port 30)  
 $wpp5831 = (wsp5831 + dpinf - dp_{prt}) / q_{calc}$  (module 58, port 31)  
 $wpp5832 = (wsp5832 + dpinf - dp_{prt}) / q_{calc}$  (module 58, port 32)

\* ***North Wall Centerline Pressures***

$wpp5901 = (wsp5901 + dpinf - dp_{prt}) / q_{calc}$  (module 59, port 1)  
 $wpp5902 = (wsp5902 + dpinf - dp_{prt}) / q_{calc}$  (module 59, port 2)  
 $wpp5903 = (wsp5903 + dpinf - dp_{prt}) / q_{calc}$  (module 59, port 3)  
 .  
 .  
 .  
 $wpp5930 = (wsp5930 + dpinf - dp_{prt}) / q_{calc}$  (module 59, port 30)  
 $wpp5931 = (wsp5931 + dpinf - dp_{prt}) / q_{calc}$  (module 59, port 31)  
 $wpp5932 = (wsp5932 + dpinf - dp_{prt}) / q_{calc}$  (module 59, port 32)

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REPORT DOCUMENTATION PAGE					Form Approved OMB No. 0704-0188	
<p>The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.</p> <p><b>PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.</b></p>						
1. REPORT DATE (DD-MM-YYYY)		2. REPORT TYPE			3. DATES COVERED (From - To)	
01-08 - 2014		Technical Memorandum				
4. TITLE AND SUBTITLE  Data Reduction Functions for the Langley 14- by 22-Foot Subsonic Tunnel				5a. CONTRACT NUMBER		
				5b. GRANT NUMBER		
				5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S)  Boney, Andy D.				5d. PROJECT NUMBER		
				5e. TASK NUMBER		
				5f. WORK UNIT NUMBER  122711.03.07.07.05.80		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) NASA Langley Research Center Hampton, VA 23681-2199				8. PERFORMING ORGANIZATION REPORT NUMBER  L-19877		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, DC 20546-0001				10. SPONSOR/MONITOR'S ACRONYM(S)  NASA		
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)  NASA/TM-2014-218513		
12. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 61 Availability: NASA CASI (443) 757-5802						
13. SUPPLEMENTARY NOTES						
14. ABSTRACT  The Langley 14- by 22-Foot Subsonic Tunnel's data reduction software utilizes six major functions to compute the acquired data. These functions calculate engineering units, tunnel parameters, flowmeters, jet exhaust measurements, balance loads/model attitudes, and model /wall pressures. The input(required) variables, the output(computed) variables, and the equations and/or subfunction(s) associated with each major function are discussed.						
15. SUBJECT TERMS Balance loads; Model attitudes; Data reduction; Engineering units; Flowmeters; Functions; Jet exhaust measurements; Model pressures; Wall pressures; Subfunctions; Tunnel parameters						
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON	
a. REPORT	b. ABSTRACT	c. THIS PAGE			STI Help Desk (email: help@sti.nasa.gov)	
U	U	U	UU	78	19b. TELEPHONE NUMBER (Include area code) (443) 757-5802	