# DEPARTMENT OF THE INTERIOR UNITED STATES GEOLOGICAL SURVEY

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#### $\mathbf{THE}$

# FRACTIONATION OF CRUDE PETROLEUM BY CAPILLARY DIFFUSION

BY

#### J. ELLIOTT GILPIN AND MARSHALL P. CRAM

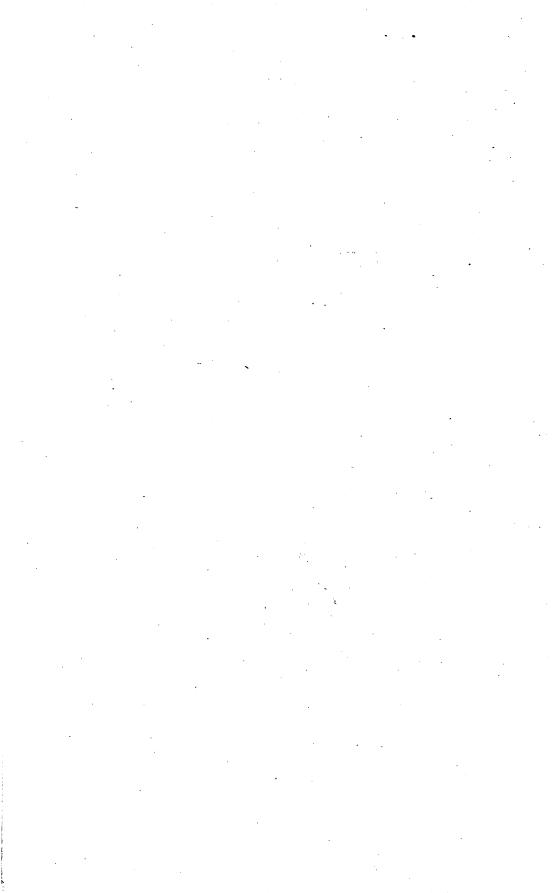
UNDER THE SUPERVISION OF

DAVID T. DAY



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# THE FRACTIONATION OF CRUDE PETROLEUM BY CAPILLARY DIFFUSION.

#### By J. ELLIOTT GILPIN and MARSHALL P. CRAM.

#### INTRODUCTION.

When, in process of refinement, black vaseline is filtered through warm, dry fuller's earth, the first product is an oil that is perfectly liquid at ordinary temperatures, but the succeeding portions are progressively more viscous until fairly hard vaseline is obtained. The observation that a fractional separation of oils in vaseline had been effected suggested to David T. Day that a like result might be obtained with crude petroleum. He applied this method to a sample of green crude petroleum from the "third sand" of Venango County, Pa., and found that light products, chiefly gasoline, first appeared when such crude oil was allowed to filter down through a long glass tube filled with granulated or powdered fuller's earth.<sup>a</sup>

This result was followed by experiments with a more elaborate system of specially constructed funnels similar to those used by the refiners of vaseline in testing the comparative value of various fuller's earths. The results from these experiments were briefly summarized in a paper on the ability of petroleum to migrate in the earth.<sup>b</sup> Engler later verified these results and showed that the separation was mechanical and that no oxidation was effected in the process. Day next used a large closed funnel of galvanized iron holding about 100 pounds of fuller's earth. When crude petroleum was dropped slowly and regularly into this funnel, rather light oils were obtained at first, followed by the usual succession of heavier oils. As it was • evident from this work that much of the oil passed through crevices without any change, Day tried the effect of reversing the route of the oil and of allowing it to diffuse upward through a tube packed tightly with fuller's earth. In such a tube the lighter constituents rose much more rapidly than the more viscous oils, so that by separat-

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a Proc. Am. Philos. Soc., vol. 36, No. 154, 1897. b Trans. Petroleum Congress (Paris), 1900.

ing the fuller's earth from different sections of the tube and displacing the oil by water, very different oils were obtained from the upper and lower parts of the tube.

By using several tubes and uniting oils of the same specific gravity oil of different grades can be collected in sufficient quantity to be fractionated again, and the process can be continued until oils result which are not altered by further passage through tubes filled with fuller's earth. At the suggestion and with the cooperation of Doctor Day we have taken up this problem with the results here stated.

#### DETAILED DESCRIPTION OF EXPERIMENTS.

#### FRACTIONATION IN TUBES.

The tubes used first were of glass, 3 feet long and  $1\frac{1}{8}$  inches in diameter. They were closed at the lower end with corks along whose sides six or seven grooves had been cut, the inner end of the cork being covered with a bit of cotton cloth to prevent the earth from sifting out through the grooves. Such tubes filled with fuller's earth were placed with their lower ends in an open dish of petroleum and the oil was allowed to rise.

At room temperatures (18° to 22° C.) and atmospheric pressure, the rate of rise of crude petroleum in a tube filled with fuller's earth was very slow. In seven days the oil ascended but 73 centimeters in one tube and 59 centimeters in another, and in a third tube ten days were required for it to rise 59 centimeters. To study the effect of heat, a glass tube about 3 feet long and 11 inches in diameter was filled with earth and placed in a bottle holding about 2 liters of oil; and the whole was heated by an electric stove with which temperatures considerably above those of the room could be maintained day and night. The temperature of the tube was kept between 40° and 70° for three days, in which time the oil rose 54.7 centimeters in the tube; in another tube packed in all ways like the first, but held at room temperature (about 20°), the oil rose 46 centimeters in the same length of time. With two tubes in which the earth was packed much less compactly the time required for the oil to rise 54 centimeters was four days for the tube at room temperature and two days . for the one at 50° to 80°. The rate of rise was evidently but little affected by heat, at least within this range of temperature, and higher temperatures could not be used without loss of the more volatile constituents of the oil.

The next attempt at increasing the rate of rise of the oil consisted in applying diminished pressure to the top of the tube, which reduced the time required for the oil to reach the top of a tube 5 feet long from several weeks to seventeen hours. If diminished pressure is continued after the oil has reached the top and if the oil is not exhausted in the reservoir at the bottom, oil will be drawn over from the top of the tube. The specific gravity of the oil thus collected steadily rises as it comes over. The samples so obtained, however, stand under very low pressures for some time, which may cause a loss of their more volatile constituents. This suggested applying increased pressure to the oil in the reservoir rather than diminished pressure to the top of the tube, and an iron bomb, like those used for the transportation of mercury, was fitted with an iron pipe 7 feet long to contain earth and a side arm at the bottom of the bomb to which a water column might be attached.

The bomb, which held about 2 liters, could be partly filled with petroleum and the pipe containing the earth screwed into the top. The side arm which opened into the bottom of the bomb could then be connected with the water pressure so that the lower part of the bomb was filled with water which drove the petroleum upward. The oil obtained at the top, however, was fractionated no further nor in any larger amounts than when the oil was not allowed to emerge from the top of the tube. The difficulty of setting up such a pressure apparatus with tight connections, as well as the range of pressure required—a column of water 7 feet high being too great when the oil was just started up the tube and a column 30 feet high being insufficient when it was near the top—made its use impracticable.

To use diminished pressure, the earth in the tubes must not be packed so hard that the air just above the oil can not be drawn through the earth above, nor must the earth be packed so loosely that the oil will rise as in a vacuum. The right degree of hardness is obtained by filling about 1 foot of the tube at a time and packing that much earth as hard as possible with a wooden rod tipped with a rubber stopper. If the tube when pounded on the floor rings in the hand, it indicates that the earth may be packed too closely. Tubes may be packed much more easily by filling several at once, with a separate ramrod for each. By allowing a few minutes to elapse between successive liftings of the ramrod, much labor is avoided. Α bit of cotton waste below a rubber stopper at the top of the tube will prevent any earth from being drawn up when the air is exhausted. The fuller's earth was first heated in shallow iron pans until it ceased to form geysers when stirred. The earth must be thoroughly cold before it is packed into tubes, or the contraction will be sufficient to allow the oil to run up the tube immediately when the air is exhausted.

Much trouble was experienced with the tubes first used on account of their breaking—not when in service, but soon afterward. This was thought to be due to the age of the tubing, but the same thing happened with new tubes 5 feet long and  $1\frac{1}{4}$  inches in diameter. With the idea that the iron scraper used to remove the earth from the tubes might be the cause, a scraper entirely of wood was tried, but this did not decrease the breakage, it being nothing unusual on going to the laboratory in the morning to find that half of the tubes which had been emptied the day before were cracked.

It had been considered necessary to use tubes of glass in order that the height to which the oil had risen could be seen and that in removing the oil from the middle of the tube it might be scraped out to a sharp dividing line, as the level to which the oil has risen is the point from which should be made all measurements of sections into which the tube is to be divided. Tin tubes were used later to avoid the trouble experienced with glass tubes. These tin tubes were emptied by shaking the earth from the bottom into four 30-centimeter cylinders of the same diameter as the tube, these cylinders being made of two curved pieces of tin held together by a cap at one end and a ring at the other. The cylinders containing the contents of the tube could be opened lengthwise and the earth divided into any desired Two glass tubes 5 feet long and 14 inches in diameter were lengths. set up in the same dish of petroleum with ten or twenty tin tubes  $5\frac{1}{2}$ feet long and of the same diameter as the glass tubes, and when the oil stood at the top of the glass tubes the tin ones were also opened. Glass tubes, of course, can be emptied as well as tin tubes by shaking the contents from the bottom, and there was no more breakage after this method was adopted.

The level to which the oil will rise can be regulated by the amount of oil in which the tube is placed, and in the later work the adoption of this method did away with the use of glass tubes entirely. In a tube  $1\frac{1}{4}$  inches in diameter and  $5\frac{1}{2}$  feet long 950 cubic centimeters of oil will rise within 20 to 35 centimeters of the top.

When the oily earth has been removed from the tube, the oil may be separated by adding water. In the first experiments enough water was added to form a very thin mud, which was thoroughly stirred by a small propeller driven by a water motor. The mixed earth, oil, and water were then poured into a large separating funnel and allowed to stand several minutes until the oil had collected at the top. The earth and water could then be drawn off and the pure oil left.

It was found later, however, that if less water is added to the earth as removed from the tubes, after standing a few minutes all the water will pass into the earth and this will be accompanied by the liberation of oil. Oil so liberated can then be poured off directly from the earth without the labor of churning. When water first begins to liberate oil, the earth is granular; but when more water has been added and the last of the oil recovered, the earth has the consistency of a thin paste that will flow when the dish is inclined, which it will not do when the oil begins to come off.

All the oil from one section of a tube is of the same color irrespective of whether it is the first or the last oil to come off when water is added. It was assumed at first that all the oil which came from one section of earth had the same specific gravity, but this was found later not to be the case. The first oil to be collected, if taken in sufficiently small volume, say about 20 cubic centimeters, is slightly heavier than the next portion. If as much as 100 cubic centimeters is included in the first sample, however, this will not be true. Beginning with the second sample the successive portions of oil steadily increase in specific gravity, the gradual addition of water affording another means of fractionation in addition to the separating power of the earth. Both of these methods of separation have been combined in this investigation. The earth must be thoroughly mixed after each addition of water to prevent a layer of water-wet earth from isolating earth that contains oil from the water added.

The petroleum used was a dark-green oil from Venango County, Pa., of specific gravity 0.810. When 950 cubic centimeters of this oil was drawn upward in a tin tube  $5\frac{1}{2}$  feet long, the following separation was obtained:

|   | ]  | l,   | 2   | 2.   | 8  | <br>3.   |
|---|--|--|---|--|--|--|
| Time required, in hours<br>Distance from top of tube to oil when<br>opened, in centimeters  |  | 3.5  | 17<br>28  | 7.5  | 17<br>28   | 7.5<br>3   |
|   | Specific<br>gravity.   | Cubic<br>centime-<br>ters.                       | Specific<br>gravity.  | Cubic<br>centime-<br>ters.                       | Specific<br>gravity.                                     | Cubic<br>centime-<br>ters.                       |
| A, 8 contineters at top<br>B, next 8 centimeters<br>C, next 18 centimeters<br>D, next 30 centimeters<br>E, next 35 centimeters<br>F, rest | $\left\{\begin{array}{c} .8125\\ .8137\\ .815\end{array}\right.$ | 42<br>45<br>75<br>24<br>130<br>170<br>125<br>611 | 0. 8012<br>. 804<br>. 807<br>. 809<br>. 8125<br>. 8185<br>. 823 | 30<br>37<br>47<br>22<br>148<br>190<br>100<br>574 | 0.8022<br>.803<br>.8075<br>.810<br>.812<br>.8175<br>.821 | 18<br>35<br>66<br>25<br>140<br>145<br>105<br>534 |

TABLE 1.—Fractionation of crude petroleum in single tubes.

The oil in grade C was collected in two portions, the second being obtained by the addition of more water after the first lot of oil was poured off. Although 950 cubic centimeters of crude petroleum were used in each experiment, it will be noticed that the oil recovered measures much less than that. When several tubes were worked up together, in one test 9,070 cubic centimeters of crude petroleum yielded 5,951 cubic centimeters of oil and in another 8,915 cubic centimeters gave 5,415 cubic centimeters.

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| • | Δ |
|---|---|
| £ | 0 |
|   |   |

TABLE 2.—First fractionation of crude petroleum.

FRACTIONATION OF CRUDE PETROLEUM.

| -  |  | 4  |   | 5.   |                                    |                                |   |   |  | ×.   |  | 6  |
|--|--|--|---|--|------------------------------------|--------------------------------|---|---|--|--|--|--|
| Tubes.<br>Distance from level of oil to top of tube,<br>In centimeters.a<br>Time required, in hours. | 2 glass, 8 tin<br>Glass, 0, 15; tin, 4<br>15, 24, 22, 28, 19, 2<br>54. | 0.4  | 2 glass, 7 tin<br>Glass, 0, 6.5; tin, 2<br>28, 18, 15, 28, 12, 2<br>24. |  |                                    | · ·                            | 2 glass, 7 tin<br>Glass, 0, 7; tin, 2<br>26, 23, 26, 28, 20,<br>84. | tin<br>7; tin, 25,<br>6, 28, 20, 28.  | 2 glass, 7 t<br>Glass, 0, 5<br>34, 28, 15<br>48. | , 7 tin 16,<br>0, 5, tin, 16,<br>3, 15, 18, 23, 10.                | 2 glass, 7<br>Glass, 8<br>58, 31, 6<br>16.<br>117. | 7 tin.<br>8.5, 15; tin,<br>60, 40, 16, 53, |
|  | Specific<br>gravity.   | Cubic cen-<br>timeters.  | Specific<br>gravity.  | Cubic cen-<br>timeters.  | Specific<br>gravity.               | Cubic cen-<br>timeters.        | Specific<br>gravity.  | Cubic cen-<br>timeters.   | Specific<br>gravity.                             | Cubic cen-<br>timeters.  | Specific<br>gravity.                               | Cubic cen-<br>timeters.                    |
| X  | 0.8015<br>8005   | 50<br>350  | 0.804<br>.8055  | 100  | 0.805                              | .200<br>200                    | 0.800<br>.802   | 200<br>115  | 0. 798<br>. 801                                  | 130  | 0.8025<br>.8037                                    | 175<br>120                                 |
| 3.   | { 807<br>810   | 260<br>190   | .8085   | 220  | . 807<br>. 8097                    | 140<br>125                     | . 8042<br>. 8048  | 200<br>200  | . 803<br>. 8045                                  | 155<br>230   | . 8042   | 180<br>215                                 |
| ¢  | 809<br>809<br>8115<br>8115   | 260<br>260<br>260<br>260<br>260<br>260<br>260<br>260<br>260<br>260 | . 8097  | 300  | . 810<br>. 8135                    | 390                            | .808<br>.8078<br>.8118  | 330<br>430<br>95  | . 8072<br>. 808<br>. 808                         | 430<br>275<br>225  | . 809<br>. 8095<br>. 8127                          | 300<br>440<br>100                          |
| D  | 815<br>8145<br>8145<br>8175  | 425<br>625<br>460  | .813<br>.8135<br>.816   | 530<br>500<br>500<br>500<br>500<br>500<br>500<br>500<br>500<br>500 | . 8133<br>. 816<br>. 8175<br>. 825 | 610<br>325<br>435<br>125       | .812<br>.812<br>.814  | 425<br>625<br>360   | 8117<br>812<br>812<br>822<br>8145<br>8145        | 420<br>580<br>300<br>42  | .812<br>.8137<br>.8145<br>.8155                    | 390<br>300<br>300<br>200                   |
| ſ  | 815  | 830<br>830<br>830<br>830<br>830<br>830<br>830<br>830<br>830<br>830 | 8162<br>8162<br>819   | 480<br>725<br>390  | .816<br>.8195<br>.821<br>.827      | 850<br>330<br>325<br>325       | .8172<br>.816<br>.8162<br>.8195                                     | 850<br>866<br>300<br>866<br>860<br>860<br>860<br>860<br>860<br>860<br>860<br>860<br>8 | 8135<br>814<br>814<br>8248<br>817<br>821         | 230<br>230<br>230<br>230<br>230<br>230<br>230<br>230<br>230<br>230 |  | 340<br>240<br>350<br>350                   |
| a The class turbs  | are 5 feet 1   | as are 5 faat long the tin tubes 54 feat                           | tuhes 54 fe   |  | a 11 inches                        | Both are 14 inches in diameter |   |   |  |  |  |  |

a The glass tubes are 5 feet long, the tin tubes 54 feet. Both are 14 inches in diameter. <sup>b</sup> Record of distance lost for two of the tin tubes. <sup>c</sup> These fractions stood uncovered on top of the earth overnight, and consequently were exposed to considerable evaporation.

TABLE 2.— First fractionation of crude petroleum—Continued.

c

|  | 10.   |   | H   | 11.a                     | H  | 12.5   | 1  | 13. c  |   | 14.   |   | 15.  |
|--|---|---|---|--------------------------|--|--|--|--|---|---|---|--|
| Tubes  | 2 glass, 9 tin<br>Glass, 0, 8.5; tin, 4<br>32, 36, 26, 27, 20, 2<br>25, 18. | in<br>5; tin, 40,<br>27, 20, 27,  | 2 glass, 8<br>Glass, 0,<br>0, 0, 20,<br>39. | 2 glass, 8 tin           | 2 glass, 6 tin<br>Glass, 7, 13; tin, 5<br>19, 32, 35, 48, 29.<br>60. | tin  | 2 glass, 9 tin<br>Glass, 2, 2.5;<br>10, 11, 22, 16<br>5.5, 14. | 2 glass, 9 tin<br>Glass, 2.25; tin.17,<br>10, 11, 22, 16, 29, 8, 5,<br>5.5, 14,                          | 2 glass, 9<br>. Glass, 0,<br>20.5, 13<br>19, 8, 12<br>16.5. | , 9 tin 20, 0, tin, 20, 13.5, 15, 14.5, 12, 14.5, 12, 14.5,                     | 2 glass, 9<br>Glass, 0,<br>31, 23, 2<br>16, 14. | 2 glass, 9 tin.<br>Glass, 0, 10; tin, 32,<br>31, 23, 23, 24, 26, 9,<br>16, 14,<br>16.75. |
|  | Specific<br>gravity.  | Cubic cen-<br>timeters.   | Specific<br>gravity.                        | Cubic cen-<br>timeters.  | Specific<br>gravity.   | Cubic cen-<br>timeters.  | Specific<br>gravity.   | Cubic cen-<br>timeters.  | Specific<br>gravity.  | Cubic cen-<br>timeters.   | Specific<br>gravity.                            | Cubic cen-<br>timeters.  |
| V  | 0. 7995<br>- 8037<br>- 806  | 200<br>730<br>730<br>730<br>730<br>730<br>730<br>730<br>730<br>730<br>7 | 0. 799<br>. 802                             | 88                       | 0. 798<br>. 801  | 150<br>140   | 0. 8015<br>. 8055<br>. 8028<br>. 8033                          | 110<br>40<br>100   | 0. 798<br>. 8005<br>. 8015                                  | 225<br>110<br>80  | 0. 800<br>. 805                                 | 300<br>95  |
| B  | . 8085<br>. 810<br>. 8112   | 125<br>275<br>23  | . 8115                                      | 200                      | . 8022<br>. 806<br>. 8072  | .160<br>105<br>20  | . 802<br>. 8072<br>. 8085<br>. 8085                            | 230<br>60<br>75  | . 8015<br>. 804<br>. 8058                                   | 210<br>150<br>120   | . 802<br>. 808<br>. 8055                        | 300<br>300<br>120  |
| C  | .810<br>.812<br>.812<br>.8135   | 350<br>525<br>150   | . 810<br>. 811<br>. 8145                    | 300<br>490<br>175        | . 807<br>. 809<br>. 8115   | 400<br>60<br>60  | . 806<br>. 808<br>. 8072<br>. 8072                             | 340<br>320<br>320<br>150   | . 8048<br>. 8065<br>. 8075                                  | 500<br>385<br>225   | . 8065<br>. 810                                 | 800<br>350   |
|  | 8148<br>8175<br>8175<br>8175<br>817<br>817                                  | 440<br>700<br>370<br>200  | . 8133<br>8133<br>816<br>. 816<br>. 8142    | 450<br>230<br>250        | .811<br>.8097<br>.811<br>.811<br>.815                                | 400<br>230<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60 | . 809<br>. 8135<br>. 8115<br>. 8115<br>. 812                   | 69<br>68<br>68<br>68<br>68<br>69<br>69<br>69<br>69<br>69<br>69<br>69<br>69<br>69<br>69<br>69<br>69<br>69 | . 810<br>. 810<br>. 810<br>. 812<br>. 812                   | 500<br>660<br>280<br>280<br>280<br>280<br>280<br>280<br>280<br>280<br>280<br>28 |   | 600<br>525<br>200<br>200   |
| Đ.   | 8197<br>8215<br>8223<br>821   | 315<br>720<br>570<br>215  | .8172<br>.818<br>.818<br>.819<br>.8175      | 400<br>520<br>405<br>370 | .815<br>.8148<br>.8148<br>.815<br>.817                               | 260<br>510<br>100  | .813<br>.818<br>.8167<br>.8167                                 | 85<br>285<br>80<br>285<br>285<br>285   | . 8135<br>. 8155<br>. 8155<br>. 8162<br>. 8162              | 470<br>530<br>680   | . 8145<br>. 820<br>. 818<br>. 818               | 740<br>400<br>820  |
| a During the night, oil was drawn entirely through and out at the top of five tubes and so was lost. | ntirely thro  | ugh and ou  | t at the to                                 | p of five tu             | bes and so   | was lost.  |  | _  |   | _   | _   |  |

b Three other tubes were set up with these, but when opened the oil in them was \$1, \$3, and 90 centimeters from the top, so they were discarded. This unevenness between the tubes was probably caused by using in some of them earth which was not entirely cold. Beginning with lot 13 the pump was run continuously day and night.
d Afficient are sets tubes are 5 feet long, the tin tubes 5 feet. Both are 14 induces in diameter.

FRACTIONATION IN TUBES.

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TABLE 2.—First fractionation of crude netroleum—Continued.

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<sup>a</sup> Two reservoirs of crude oil were used in each of lots 18 and 19, but the earth from all 22 tubes was worked up together. Section D from all 22 tubes was first united and then, for convenience in working, divided into two portions. <sup>b</sup> The glass tubes are 5 feet long, the tin tubes 5§ feet. Both are 1§ inches in diameter.

FRACTIONATION OF CRUDE PETROLEUM.

To collect a sufficient quantity of oil, several tubes were placed in the same container of petroleum, two of the tubes being of glass and the rest of tin. When the oil had reached the top of the glass tubes all the tubes were opened, and the earth from the same level in all the tubes was mixed in tin pails. The oil was then liberated in several successive fractions by the addition of successive amounts of water. If the earth had been thoroughly mixed after each addition of water, the various oils from the same lot of earth would have increased regularly in specific gravity, instead of showing the variations which they did. For example, the first oil to be displaced by water in grades D and E of lot 4 (Table 2), with so large a volume, would not have been heavier than the succeeding oils if the water and earth had been thoroughly mixed before the oil was poured off. If we were to repeat the work, instead of using one common reservoir for all the tubes, we should use a separate reservoir for each tube, and open the tube when the oil in the reservoir was exhausted. This would do away entirely with the use of glass tubes, besides insuring that the level of the oil in each tube when opened would be practically the same. If a common reservoir is to be used, the tubes should all be packed with practically the same degree of hardness if the oil is to ascend in all with equal rapidity, as the ascent in all tubes is checked at the same time-that is, when the oil in the reservoir is exhausted.

Diminished pressure was obtained by the use of a Chapman water pump, which reduced the pressure to 5 to 12 centimeters Hg., when connected with a system of tubes. In the earlier work the pump was not run through the night, which accounts for the much longer time required for these lots of tubes.

The earth from a tube was divided into six sections, the level to which the oil had ascended in the tube being taken as the point to be measured from. A, the top section, included the 8 centimeters next the top; B, the next 8 centimeters; C, the next 18; D, the next 30; E, the next 35; and F what earth was left. F varied, of course, depending on the height to which the oil had risen. In fractionating the crude petroleum in bulk, F was usually discarded, as it was so viscous that it was deemed impossible to pass it through earth again. Records from several lots of tubes are given in Table 2. The specific gravity was measured with a Westphal balance, the temperature of the oil being in every case exactly 20° C. Although the fourth decimal place is not to be taken as strictly accurate, yet it is considered worth while to record it as giving a nearer approach to the truth than would result from the use of only three decimal places.

To study further the fractionation on addition of water, the oil of grade E from lot 16 was collected in fourteen fractions. The weight of the earth impregnated with oil before any water had been added was 13.5 pounds, and the weight of the earth containing all the water added, but minus the oil, was 17.5 pounds. The earth was placed in a galvanized-iron garbage pail and the water stirred in with an iron paddle. When the first portion of oil was liberated, the mass was of the consistency of bran, but as more water was added it turned to a fluid paste. When water was added and the pail inclined, oil would continue to drain out for half an hour or longer before the addition of more water became necessary. The oil which was liberated by one lot of water, therefore, could be collected in several portions, and this was done to see whether the oil which comes off immediately after the addition of water is the same as that which drains out later. The letters I, II, etc., indicate that the fractions included were liberated by one addition of water.

| · . | Specific<br>gravity.  | Cubic<br>centi-<br>meters. |    | Specific<br>gravity.   | Cubic<br>centi-<br>meters. |
|-----|---|----------------------------|----|--|----------------------------|
| п   |   | 25<br>70<br>70<br>250      | IV | $\begin{cases} 0.8208 \\ .8222 \\ \\ .824 \\ .828 \end{cases}$ | 575<br>55<br>170<br>16     |
| ш   | $\left\{\begin{array}{c} .818\\ .318\\ .818\\ .820\end{array}\right.$ | 395<br>350<br>460<br>60    | vI | { . 827<br>. 830   | 95<br>45                   |

TABLE 3.—Fractionation of oil of grade E, lot 16, Table 2.

The first fraction is regularly of higher specific gravity than those immediately following if only enough water is added to liberate a first fraction of small volume, say about 20 cubic centimeters. As the fraction first obtained becomes larger in volume, it approaches nearer to the second fraction in specific gravity, and will even fall below that fraction if the volume is made too large.

The range of specific gravity covered by this first fractionation of the crude petroleum of specific gravity 0.810 was from 0.800 to 0.830. Fractions of the same specific gravity and of the same grade were united and the products chilled and filtered to remove all the dissolved paraffin possible. This was done out of doors toward the last of December, when the thermometer stood at about 4° to 8° C. Lower temperatures would not only throw paraffin out of solution, but cause the whole oil to thicken. The oils were filtered through large plaited filters of drying paper, twenty-four hours or more being required for many of the filters to empty completely. The lighter oils in sections A and B deposited no paraffin. Some of the heavier grades deposited as much as 10 per cent of their weight, accompanied in many cases by a slight change in specific gravity.

When these oils were filtered through earth again they behaved as shown in Table 4. As before, 950 cubic centimeters of each oil was used and the tube was divided into five sections, A being the top 8 centimeters, B the next 8, C the next 18, D the next 30, and EF the rest.

#### TABLE 4.—Second fractionation.

[NOTE.—Nine hundred and fifty cubic centimeters were needed for each tube, and for many tubes this amount was available of the same grade (A, B, C, etc.) and of the same specific gravity. For some tubes, however, it was necessary to unite oils of the same grade which differed slightly in specific gravity. No such samples differed by more than 0.0015 and all are marked with an asterisk (\*) in the table.]

|                         | 20 (A,   | 0.8015).   | 21 (A,  | 0.806).  | *22 (B  | , 0.805).                            | 23 (B,   | 0.8055).                                  |
|-------------------------|--|--|---|--|---|--------------------------------------|--|---|
|                         | Specific<br>gravity.   | Cubic<br>centime-<br>ters.   | Specific<br>gravity.  | Cubic<br>centime-<br>ters.   | Specific<br>gravity.                            | Cubic<br>centime-<br>ters.           | Specific<br>gravity.                                     | Cubic<br>centime-<br>ters.                |
| A<br>B<br>C<br>D        | $\begin{cases} 0.8012 \\ .800 \\ .8012 \\ .8027 \\ .8022 \end{cases}$                        | 36<br>44<br>68<br>35<br>170  | 0. 8038<br>. 8035<br>. 8035<br>. 8052<br>. 805                                      | 45<br>48<br>78<br>28<br>160  | 0. 7997<br>. 802<br>. 8055<br>. 8063            | 50<br>50<br>108<br>175               | 0. 8005<br>. 8033<br>. 805<br>. 8063                     | 45<br>48<br>115<br>180                    |
| ĔF                      | . 8047   | 330<br>683   | . 807   | 320<br>679   | . 808   | 260<br>643                           | . 8085   | 260<br>648                                |
|                         | 24 (B,   | 0.8065).   | 25 (B,  | 0.809).  | *26 (B  | , 0. 8105).                          | *27 (B   | , 0. 812).                                |
| ABBB                    | 0. 8077<br>. 807<br>{ . 808<br>. 8092<br>. 8115  | 38<br>50<br>80<br>160<br>300<br>628  | 0. 8013<br>. 805<br>. 807<br>. 810<br>. 8095<br>. 8115                              | 45<br>50<br>75<br>30<br>180<br>350<br>730  | 0. 8075<br>. 8085<br>. 8105<br>. 8125<br>. 8133 | 38<br>50<br>100<br>160<br>275<br>523 | 0. 8105<br>. 8105<br>. 8085<br>. 810<br>. 8115<br>. 8145 | 42<br>42<br>73<br>22<br>140<br>250<br>569 |
|                         | 28 (C,   | 0.8095).   | 29 (Ċ,  | 0. 810).   | 30 (C,  | 0. 811).                             | *31 (C,  | 0. 811).                                  |
| ABC<br>D<br>EF          | 0. 805<br>. 8065<br>{ . 8085<br>{ . 811<br>{ . 811<br>. 813                                  | 52     52     70     28     160     350     712     712                    | 0. 8035<br>. 808<br>. 810<br>. 8115<br>. 8115<br>. 8135<br>. 813                    | $ \begin{array}{r} 40 \\ 40 \\ 75 \\ 30 \\ 140 \\ 40 \\ 350 \\ \hline 715 \\ \end{array} $ | 0. 8005<br>. 809<br>. 812<br>. 813<br>. 8145    | 50<br>38<br>115<br>175<br>310<br>688 | 0. 803<br>. 808<br>. 813<br>. 8135<br>. 8155             | 50<br>55<br>105<br>180<br>300<br>690      |
|                         | 32 (C, 0.8115).  |  | 33 (C, 0.813).  |  | *34 (C, 0.8135).                                |                                      | *35 (C, 0.8135).   |   |
| AB                      | 0. 806<br>. 807<br>{ . 810<br>. 812<br>{ . 812<br>. 813<br>. 813<br>. 8135<br>. 813<br>. 813 | · 45<br>35<br>60<br>33<br>33<br>70<br>97<br>103<br>105<br>50<br>47<br>a 63 | 0. 8072<br>. 811<br>. 812<br>. 813<br>. 8145<br>. 8155<br>. 8155<br>. 8155<br>. 818 | 20<br>35<br>70<br>25<br>90<br>80<br>200<br>125<br>35                                       | 0. 803<br>. 810<br>. 813<br>. 815<br>. 817      | 42<br>53<br>100<br>150<br>300        | 0. 8025<br>. 8077<br>. 8135<br>. 8145<br>. 817           | 35<br>35<br>100<br>160<br>325             |
|                         | <br>   | 708  | <br>  | 680  |   | 645                                  |  | 655                                       |
|                         | 36 (C,   | 0.815).  | *37 (C,   | 0.8155).   | *38 (C,   | 0.8155).                             | *39 (C,  | 0.8165).                                  |
| A<br>B<br>C<br>D<br>E F | 0.805<br>.8105<br>.814<br>.815<br>.817   | 43<br>40<br>98<br>155<br>280   | 0.8053<br>.812<br>.816<br>.8175<br>.819   | 50<br>45<br>103<br>160<br>310  | 0.808<br>.8095<br>.8135<br>.817<br>.819         | 40<br>50<br>100<br>165<br>290        | 0. 808<br>. 8145<br>. 816<br>. 8175<br>. 820             | 50<br>50<br>82<br>125<br>310              |
|                         |  | 616  |   | 668  |   | . 645                                |  | 617                                       |

a Unused.

#### FRACTIONATION OF CRUDE PETROLEUM.

|                        | *40 (D,   | 0.8135).                      | 41 (D,                                       | 0.814).                       | 42 (D,  | 0.814).   | 43 (D,  | 0.814).                                      |
|------------------------|---|-------------------------------|--|-------------------------------|---|---|---|--|
|                        | Specific gravity.   | Cubic<br>centime-<br>ters.    | Specific<br>gravity.                         | Cubic<br>centime-<br>ters.    | Specific<br>gravity.  | Cubic<br>centime-<br>ters.                            | Specific<br>gravity.  | Cubic<br>centime-<br>ters.                   |
| A<br>B<br>C            | 0. 8095<br>. 8085<br>{ . 811  | 45<br>45<br>95                | 0. 8045<br>. 8115<br>. 8135<br>. 8165        | 30<br>45<br>75<br>28          | 0. 806<br>. 811<br>. 813  | 32<br>45<br>92  | 0. 806<br>. 8097<br>. 814   | 25<br>30<br>50                               |
| D<br>EF                | . 8155<br>. 817   | 165<br>320                    | . 8105<br>. 818<br>. 821                     | 140<br>300                    | . 8175<br>. 8195  | 140<br>310  | . 8157<br>. 8175  | 145<br>400                                   |
|                        |   | 670                           |  | 618                           |   | . 619   |   | 650  |
|                        | 44 (D,  | 0.814).                       | 45 (D,                                       | 0.814).                       | 46 (D,  | 0.8145).  | 47 (D,  | 0.815).                                      |
| A<br>B<br>C<br>D<br>EF | $\left\{\begin{array}{c} 0.\ 8008\\ .\ 8077\\ .\ 814\\ \\ .\ 8175\\ \\ .\ 819\\ \end{array}\right.$ | 45<br>50<br>103<br>160<br>310 | 0. 800<br>. 8065<br>. 8125<br>. 816<br>. 817 | 50<br>55<br>100<br>160<br>300 | 0.808<br>8115<br>8135<br>8155<br>8155<br>817<br>818<br>818<br>8195<br>8202<br>821 | 45<br>40<br>65<br>30<br>105<br>58<br>180<br>120<br>53 | 0. 800<br>. 807<br>. 814<br>. 816<br>. 819  | 42<br>47<br>110<br>150<br>330                |
| ·····                  |   | 668                           |  | 665                           |   | 696   |   | 679  |
|                        | 48 (D,  | 0.815).                       | 49 (D,                                       | 0.8155).                      | 50 (D,  | 0.8155).  | 51 (D,  | 0.8155).                                     |
| A<br>B<br>C<br>D       | 0. 810<br>. 805<br>. 812<br>. 817<br>. 819  | 37<br>47<br>105<br>160<br>300 | 0. 8045<br>. 811<br>. 815<br>. 8185<br>. 820 | 40<br>48<br>98<br>160<br>310  | 0. 8105<br>. 8148<br>. 810<br>. 815<br>. 819                                      | 45<br>47<br>100<br>140<br>400                         | $\begin{array}{c} 0.\ 8058\\ 810\\ 8132\\ 8145\\ 8172\\ 8188\\ 8188\\ 8188\\ 820\\ 819\\ \end{array}$ | 40<br>40<br>50<br>75<br>55<br>38<br>38<br>38 |
| EF                     |   |                               |  |                               |   |   | . 8208<br>. 8208<br>. 8208<br>. 8208<br>. 8208  | 100<br>30<br>41<br>30<br>91<br>04            |
|                        |   | 649                           | ].   | 656                           |   | 732   |   | 736  |
|                        | 52 (D, 0.816).  |                               | *53 (D                                       | , 0.816).                     | 54 (D,  | 0.8165).  | 55 (D,  | 0.8165).                                     |
| A<br>B<br>C            | 0. 806<br>. 8115<br>{ . 814<br>. 814  | 38<br>42<br>70                | 0. 803<br>. 8105<br>. 815                    | 43<br>30<br>100               | 0. 806<br>. 811<br>. 815  | 47<br>48<br>98  | 0. 8095<br>. 8135<br>. 8145   | 42<br>40<br>77                               |
| D<br>EF                | . 8175<br>. 8185<br>. 821   | 25<br>125<br>300              | . 8185<br>. 820                              | 175<br>290                    | . 8188<br>. 8208  | 150<br>300  | . 8188<br>. 821   | 150<br>295                                   |
|                        |   | 700                           |  | 638                           |   | 643   | <u> </u>  | . 604  |
|                        | * 56 (D   | 0.8165).                      | *57 (D                                       | , 0.817).                     | *58 (D  | , 0.818).   | 59 (D,  | 0.8187).                                     |
| A<br>B<br>C<br>D<br>EF | $\begin{array}{c} 0.\ 806\\ .\ 810\\ .\ 8145\\ .\ 8185\\ .\ 821\end{array}$                         | 45<br>45<br>95<br>160<br>295  | 0. 8075<br>. 8115<br>. 815<br>. 818<br>. 821 | 40<br>40<br>100<br>130<br>330 | 0.808<br>.8135<br>.817<br>.820<br>.822  | 45<br>45<br>105<br>150<br>300                         | 0. 811<br>. 812<br>. 814<br>. 819<br>. 823  | 40<br>45<br>92<br>150<br>305                 |
|                        |   | 640                           |  | 640                           |   | 645   |   | 632  |

TABLE 4.—Second fractionation—Continued.

a Unused.

#### FRACTIONATION IN TUBES.

|                         | *60 (D,   | 0.8205).  | 61 (E,                                   | 0.814).                      | *62 (E,                                   | 0.8163).  | *63 (E                                   | , 0.817).                    |
|-------------------------|---|---|--|------------------------------|---|---|--|------------------------------|
|                         | Specific<br>gravity.  | Cubic<br>centime-<br>ters.                                      | Specific<br>gravity.                     | Cubic<br>centime-<br>ters.   | Specific<br>gravity.                      | Cubic<br>cent.me-<br>ters.  | Specific<br>gravity.                     | Cubic<br>centime-<br>ters.   |
| A<br>B<br>C             | 0. 8045<br>. 813<br>∫ . 8175  | 45<br>45<br>90  | 0. 8075<br>. 810<br>. 8125               | 33<br>35<br>80               | 0. 8155<br>. 808<br>. 8095                | 42<br>50<br>70  | 0. 804<br>. 8075<br>. 8145               | 44<br>50<br>102              |
| D                       | . 822   | 170   | . 818                                    | 125                          | $     . 812 \\     . 8175 \\     . 8182 $ | 25<br>105<br>32   | . 8205                                   | 150                          |
| EF                      | . 823   | 270<br>a 70   | . 8245                                   | 300                          | . 823                                     | 250   | . 8245                                   | 30                           |
|                         | ď   | 692   |  | 573                          |   | · 615   |  | 64                           |
|                         | *64 (E  | , 0.817).   | . *65 (E,                                | 0.818).a                     | *66 (E, 0                                 |   | 67 (E;                                   | 0.818).                      |
| Α                       | { 0.805   | 42  | 0. 8065                                  | 90<br>20                     | 0. 805                                    | 38  | 0. 805                                   | 40                           |
| B<br>C                  | .810<br>∫.8145  | 42<br>75  | . 810<br>. 8155                          | 110<br>186                   | $.811 \\ .8135$                           | 38<br>104   | . 811<br>. 8145                          | 4                            |
| D                       | 820   | 135   | . 817<br>. 8205<br>. 8205                | 50<br>385<br>75<br>650       | . 819                                     | 175   | . 8185                                   | . 12                         |
| EF                      | . 8255  | 235   | . 8255                                   | 650<br>260                   | . 8235                                    | 240   | . 824                                    | 32                           |
| . •                     |   | 529   |  | 1,826                        |   | 695   |  | 620                          |
|                         | *68 (E,   | 0.8185).  | 69 (E,                                   | 0.81 <u>9</u> ).             | 70 (E,                                    | 0.819).   | *71 ·(E                                  | , 0.819).                    |
| A<br>B<br>C             | $\left\{\begin{array}{c} 0.8205\\ .8043\\ .810\\ .812\end{array}\right.$  | $15 \\ 35 \\ 60 \\ 30$  | 0. 804<br>. 808<br>. 8145                | 24<br>40<br>85               | 0. 8115<br>. 814<br>. 815                 | 21<br>31<br>90  | 0. 8095<br>. 8085<br>. 814               | 23<br>34<br>80               |
| D<br>EF                 | . 817<br>. 8225   | $\begin{array}{c} 160 \\ 300 \end{array}$                       | . 8195<br>. 824                          | 140<br>330                   | .8165<br>.824                             | 120<br>330  | . 820<br>. 824                           | 160<br>280                   |
|                         |   | 590   |  | 589                          |   | 592   |  | 57                           |
|                         | *72 (E,   | 0.8195).  | *73 (E, 0.8195).                         |                              | 74(E,0.8195).                             |   | 75 (E, 0.8197).                          |                              |
| A<br>B<br>C             | $ \left. \begin{array}{c} 0.8145 \\ .8105 \\ \left\{ \begin{array}{c} .8135 \end{array} \right. \right. \right. $ | 30<br>42<br>103   | 0. 8055<br>. 811<br>. 8155               | 34<br>45<br>80               | 0.816<br>.8135<br>.809<br>.814            | 40 <sup>°</sup><br>42<br>65<br>34   | 0.8025<br>.8105<br>.816                  | 40<br>38<br>90               |
| D<br>EF                 | $\left\{ \begin{array}{c} .8195\\ .824 \end{array} \right\}$  | $     \begin{array}{r}       160 \\       285     \end{array} $ | . 820<br>. 824                           | $120 \\ 290$                 | . 8185<br>. 824<br>. 827                  | $     \begin{array}{r}       160 \\       260 \\       30     \end{array} $ | . 822<br>. 8255                          | 150<br>300                   |
|                         |   | 620   |  | 569                          |   | 631   |  | 618                          |
| •                       | *76 (E  | , 0.820).   | *77 (E,                                  | 0.8205).                     | 78 (E,                                    | 0.8215).  | *79 (E,                                  | 0.822).                      |
| A<br>B<br>C<br>D<br>E F | 0.8045<br>.812<br>.817<br>.822<br>.826  | 48<br>40<br>91<br>155<br>260                                    | 0.806<br>.8125<br>.8175<br>.823<br>.8245 | 32<br>45<br>90<br>100<br>330 | 0.8045<br>.8135<br>.8185<br>.823<br>.8275 | 28<br>36<br>78<br>150<br>300  | 0.8105<br>.8145<br>.819<br>.8225<br>.827 | 32<br>42<br>77<br>155<br>280 |
|                         |   | 594   |  | 597                          |   | 592   |  | 580                          |

a Three tubes.

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#### FRACTIONATION OF CRUDE PETROLEUM.

|                        | 80 (E,   | 0.822).   | 81 (E,  | 0.822).   | 82 (E,   | 0.824).  | * 83 (A-1  | 3, 0.804).  |
|------------------------|--|---|---|---|--|--|--|---|
|                        | Specific<br>gravity.   | Cubic<br>centime-<br>ters.  | Specific<br>gravity.  | Cubic<br>centime-<br>ters.  | Specific<br>gravity.   | Cubic<br>centime-<br>ters.                                     | Specific<br>gravity.   | Cubic<br>centime-<br>ters.                                |
| A                      | $\left\{\begin{array}{c} 0.817\\ 810\\ 8153\\ 8163\\ 8225\\ 8225\\ 8265\\ \end{array}\right.$  | $ \begin{array}{r} 30 \\ 40 \\ 42 \\ 160 \\ 295 \\ \hline 613 \end{array} $ | 0. 8083<br>. 814<br>. 8185<br>. 824<br>. 8265                     | 26<br>40<br>92<br>140<br>270<br>568                               | 0. 8125<br>. 8127<br>. 818<br>. 819<br>. 8245<br>. 828<br>. 830          | 48<br>48<br>53<br>50<br>175<br>200<br>90<br><i>a</i> 50<br>714 | 0.803<br>.8035<br>.8035<br>.804<br>.806                                  | 32<br>25<br>63<br>14(<br>275<br>535                       |
|                        | * 84 (A-B  | 3, 0.8065).   | * 85 (A-]   | B, 0.808).  | *86 (B-C-  | D,0.8125).   | *87(B-C-   | D,0.8125).  |
| A<br>B<br>C<br>D       | $\left\{\begin{array}{c} 0.\ 8035\\ .\ 8055\\ .\ 809\\ .\ 8085\end{array}\right.$  | - 40<br>40<br>80<br>155   | 0.8085<br>.807<br>.8065<br>.8085                                  | 30<br>30<br>92<br>115   | 0.805<br>.808<br>.813<br>.815  | 32<br>42<br>85<br>175  | $\begin{array}{r} 0.805 \\ .8085 \\ .812 \\ .813 \\ .815 \end{array}$    | 80<br>73<br>118<br>75<br>285                              |
| EF                     | . 811  | 300<br>615  | . 8115  | 330<br>597  | . 820  | 280<br>614   | . 8175   | 520<br>1,151  |
|                        | * 88 (C-D-   | -F, 0.813).   | * 89 (C–D-  | E, 0.813).  | <br> *90(B-C-  | ہ (D,0.8145  | *91 (D-F   | , 0.815).d  |
| A<br>B<br>C<br>D       | { 0.8035<br>} .808<br>} .8115<br>.813<br>.8155   | 40<br>40<br>73<br>30<br>160   | 0.8035<br>.807<br>.8077<br>.8125<br>.813<br>.815<br>.815<br>.8175 | $ \begin{array}{r} 130\\20\\160\\.\\330\\60\\550\\90\end{array} $ | 0.8065<br>.808<br>.809<br>.8115<br>.813<br>.815<br>.815<br>.815<br>.8175 | $130 \\ 27 \\ 137 \\ 20 \\ 305 \\ 40 \\ 560 \\ 75$             | 0.801<br>.8025<br>.8075<br>.8085<br>.812<br>.812<br>.812<br>.817<br>.817 | 165<br>176<br>200<br>156<br>330<br>512<br>340<br>800      |
| EF                     | $\left\{ \begin{array}{c} .8195 \\ \end{array} \right\}$   | 290   | .8175<br>.818   | 830<br>425  | .8175  | 775<br>410   | .817<br>.8215<br>etc.  | $\left. \begin{array}{c} 150\\ 2,73 \end{array} \right\}$ |
|                        |  | 633   |   | 2, 595  |  | 2, 479   |  | 5, 568  |
|                        | *92 (D-E   | , 0.8163). e  | 93 (F,  | 0.822).   | 94 (F,   | 0.822).  |  |   |
| A<br>B<br>C<br>D<br>EF | $\left\{\begin{array}{c} 0.805\\ .8075\\ .8075\\ .8115\\ .815\\ .816\\ .820\\ .820\\ .8225\\ .8225\\ .8225\\ .8225\\ \end{array}\right.$ | 84<br>20<br>100<br>205<br>45<br>350<br>102<br>500<br>480<br>1,906           | 0. 8107<br>. 810<br>. 814<br>. 816<br>. 8215<br>. 8285<br>. 831   | 35<br>43<br>70<br>25<br>156<br>250<br>60<br>639                   | 0.804<br>.808<br>.8165<br>.817<br>.8218<br>.831                          | 28<br>• 37<br>63<br>30<br>146<br>255<br>559                    |  |   |
| a Lef                  | t.<br>o tubes.   |   | Four tube<br>Nine tube  |   | !e   | Three tub  | es.  |   |

TABLE 4.—Second fractionation—Continued.

To chill and filter these products of two fractionations would have entailed too much loss. As it was, much uniting of samples which differed but slightly from one another was necessary to obtain sufficient oil for further fractionation. A list of the unions which were made is given in Table 5.

#### FRACTIONATION IN TUBES.

|             |                      |   |                    |                                      |                            | Fra         | actions uni               | ited.                      |              |                           |                               |
|-------------|----------------------|---|--------------------|--------------------------------------|----------------------------|-------------|---------------------------|----------------------------|--------------|---------------------------|-------------------------------|
| Lot.        | Specific<br>gravity. | G | rade.              | Specific<br>gravity.                 | Cubic<br>centi-<br>meters. | Grade.      | Specific<br>gravity.      | Cubic<br>centi-<br>meters. | Grade.       | Specfic<br>gravity.       | Cubic<br>centi-<br>meters.    |
| 95          | 0. 805               | { | · B<br>C<br>A<br>C | 0. 8033<br>. 8035<br>. 8045<br>. 805 | 48<br>63<br>150<br>115     | A<br>A<br>A | 0. 8035<br>. 804<br>. 805 | 240<br>65<br>360           | B<br>B<br>B  | 0. 8035<br>. 804<br>. 805 | 25<br>14(<br>95<br>1, 251     |
| 96          | .807 。               | { | A<br>A<br>A        | . 8058<br>. 8065<br>. 807            | 40<br>240<br>53            | A<br>B<br>C | . 806<br>. 8065<br>. 807  | 235<br>100<br>75           | EF<br>D<br>C | . 806<br>. 8063<br>. 8065 | 275<br>180<br>92              |
| 97          | . 8085               | { | B<br>A             | . 808<br>. 809                       | 767<br>20                  | C<br>C      | . 808<br>. 809            | 80<br>210                  | A<br>A       | . 8083<br>. 8085          | 1, 290<br>20<br>118<br>1, 221 |
| 98          | . 8085               | { | A<br>A             | . 8072<br>. 8077                     | 20<br>38                   | A<br>B      | . 8075<br>. 8075          | 290<br>480                 | D            | . 8075                    | 270                           |
| 99          | . 8105               | { | A<br>C<br>C        | . 8105<br>. 811<br>. 8105            | 70<br>115<br>270           | A<br>A<br>B | . 8115<br>. 811<br>. 8115 | 21<br>40<br>308            | B<br>C       | . 811<br>. 8115           | 580<br>73<br>1, 477           |
| 100         | . 8115               |   | EF                 | . 8113                               | <b>300</b>                 | EF          | . 8115                    | 920                        |              |                           |                               |
| 101         | . 8125               |   | С                  | . 8123                               | 520                        | D           | . 8125                    | 1,220                      | EF           | . 8125                    | 820                           |
| 103         | . 8135               | { | B<br>B             | . 8125<br>. 8135                     | 180<br>106                 | B<br>C      | . 813<br>. 8135           | 45<br>925                  | С            | . 8132                    | 60<br>1, 316                  |
| 104         | . 814                |   | D                  | . 8135                               | 370                        | EF          | . 8135                    | 715                        |              |                           |                               |
| 106         | . 8145               |   | D                  | . 814                                | 500                        | с           | . 8145                    | 910                        |              |                           |                               |
| <b>1</b> 12 | . 8175               | { | C<br>C             | . 8165<br>. 8175                     | 258<br>200                 | D           | . 817                     | 425                        | D            | . 8172                    | 75<br>958                     |
| 115         | . 819                |   | D                  | 8175                                 | 305                        | D           | . 818                     | 990<br>1, 295              |              |                           |                               |
| 116         | . 819                |   | ·EF                | . 8185                               | 845                        | EF          | . 819                     | 683                        |              |                           |                               |
| 120         | . 820                |   | D                  | . 8195                               | 475                        | D           | . 820                     | 600                        |              |                           |                               |
| 123         | . 822                |   | EF                 | . 8215                               | 700                        | Ď           | . 8218                    | 460                        | EF           | . 822                     | 300                           |
| 126         | . 824                |   | D                  | . 823                                | 250                        | EF          | . 8235                    | 860                        | D            | . 824                     | 1,100                         |

#### TABLE 5.—Products of two fractionations united for the third fractionation.

No uniting was necessary for lots 102, 105, 107-111, 113, 114, 117-119, 121, 122, 124, 125, and 127. In the third fractionation, 950 cubic centimeters of each of these lots was filtered through earth again, with the results shown in Table 6.

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|                         | 95 (A-D   | , 0.805).   | 96 (A-E   | F, 0.807).  | 97 (A-C  | , 0.8085).                                | 98 (A-D  | , 0.8085).   |
|-------------------------|---|---|---|---|--|---|--|--|
|                         | Specific<br>gravity.  | Cubic<br>centi-<br>meters.  | Specific<br>gravity.  | Cubic<br>centi-<br>meters.  | Specific<br>gravity.   | Cubic<br>centi-<br>meters.                | Specific<br>gravity.                                     | Cubic<br>centi-<br>meters.                                       |
| AB                      | $\left\{\begin{array}{c} 0.\ 8065\\ .\ 805\\ .\ 804\\ .\ 805\\ .\ 8055\\ .\ 808\end{array}\right.$    | 33<br>33<br>62<br>40<br>150<br>315  | 0. 8045<br>. 806<br>. 8065<br>. 8083<br>. 808<br>. 8095       | 37<br>38<br>65<br>25<br>142<br>250  | 0. 806<br>. 8068<br>. 807<br>. 8095<br>. 8093<br>. 812             | 40<br>40<br>58<br>18<br>154<br>295        | 0.8047<br>8052<br>808<br>8093<br>8095<br>811             | 38<br>38<br>70<br>30<br>132<br>332                               |
|                         |   | 633   |   | 557   |  | 605                                       | •  | 643  |
|                         | 99 (A-C,  | 0.8105).  | 100 (EF   | , 0.8115).  | 101 (C-EI  | F, 0.8125).                               | 102 (C,  | 0.813).  |
| A<br>B<br>C<br>D<br>EF  | $\left\{\begin{array}{c} 0.8105\\ .810\\ .8075\\ .8085\\ .811\\ .814\end{array}\right.$               | 33<br>36<br>71<br>17<br>115<br>300  | 0. 8065<br>. 809<br>. 810<br>. 812<br>. 812<br>. 812<br>. 815 | 30<br>36<br>60<br>20<br>136<br>315  | 0.808<br>.8085<br>.811<br>.8145<br>.8145<br>.8145<br>.817          | 33<br>34<br>54<br>22<br>162<br>295        | 0.806<br>.8105<br>.8105<br>.813<br>.813<br>.813<br>.8157 | $ \begin{array}{c} 26 \\ 33 \\ 50 \\ -17 \\ 136 \\ \end{array} $ |
|                         |   | 572   |   | 597   | <br>   | 600                                       |  | 627  |
|                         | 103 (B-C  | , 0.8135).  | 104 (D-E  | CF, 0.814).   | 105 (C,  | 0.814).                                   | 106 (C-I   | 9, 0.8145).  |
| A<br>B<br>C<br>D<br>EF  | $\left\{\begin{array}{c} 0.8065\\ .810\\ .8135\\ .8165\\ .8165\\ .815\\ .817\end{array}\right.$       | $     \begin{array}{r}       28 \\       33 \\       60 \\       18 \\       150 \\       325 \\       \hline       614     \end{array} $ | 0.8042<br>.8115<br>.8125<br>.8147<br>.8147<br>.815<br>.819    | 35<br>36<br>60<br>28<br>175<br>230<br>564   | 0. 804<br>. 810<br>. 8142<br>. 816<br>. 8163<br>. 8185             | 40<br>40<br>58<br>25<br>270<br>280<br>713 | 0. 803<br>. 810<br>. 8145<br>. 816<br>. 816<br>. 8185    | 33<br>40<br>54<br>22<br>150<br>260<br>                           |
| · · ·                   | 107 (D  | , 0.815).   | 108 (EF   | , 0.8155).  | 109 (D,  | 0.8163).                                  | ن<br>110 (ن  | , 0.817).  |
| AB<br>B<br>C<br>D<br>EF | $\left\{\begin{array}{c} 0.\ 8035\\ .\ 8115\\ .\ 815\\ .\ 8177\\ .\ 8175\\ .\ 8195\end{array}\right.$ | 45<br>47<br>85<br>30<br>156<br>300<br>- 663   | 0.809<br>.811<br>.815<br>.815<br>.8165<br>.8165<br>.8185      | 52<br>47<br>55<br>40<br>170<br>255<br>619   | 0. 810<br>. 8105<br>. 8132<br>. 8145<br>. 8185<br>. 8185<br>. 8215 | 33<br>45<br>55<br>33<br>140<br>275<br>531 | 0. 8065<br>. 8125<br>. 817<br>. 818<br>. 8195<br>. 821   | 35<br>40<br>68<br>30<br>145<br>290<br>608                        |
|                         | 111 (EF   | °, 0.817).  | 112 (C-D  | , 0.8175).  | 113 (EF  | , 0.8175).                                | 114 (EF  | , 0.8187).   |
| AB<br>B<br>C<br>D<br>EF | $\left\{\begin{array}{c} 0.\ 8043\\ .\ 8105\\ .\ 8152\\ .\ 816\\ .\ 8182\\ .\ 8205\end{array}\right.$ | $     \begin{array}{r}       30 \\       32 \\       65 \\       43 \\       160 \\       290 \\       \hline       620     \end{array} $ | 0. 8145<br>. 811<br>. 8165<br>. 818<br>. 819<br>. 822         | $     \begin{array}{r}       35 \\       32 \\       60 \\       30 \\       150 \\       245 \\       \overline{552}     \end{array} $ | 0. 8065<br>. 812<br>. 8155<br>. 8175<br>. 8185<br>. 8185<br>. 8225 | 35<br>48<br>75<br>18<br>150<br>283<br>609 | 0. 817<br>. 8065<br>. 8122<br>. 813<br>. 8175<br>. 822   | 30<br>25<br>30<br>15<br>150<br>340<br>590                        |
|                         | 115 (D  | , 0.819).   | 116 (EI   | F, 0.819).  | 117 (D   | , 0.819).                                 | 118 (EI  | F, 0.819).   |
| A<br>B<br>C<br>D<br>EF  | 0. 8055<br>. 807<br>{ . 816<br>. 817<br>. 820<br>. 8225   | 16<br>Lost.<br>43<br>30<br>130<br>300   | 0.8032<br>.8115<br>.816<br>.820<br>.8205<br>.8235             | $     \begin{array}{r}       30 \\       36 \\       52 \\       21 \\       160 \\       240 \\       539     \end{array} $            | 0. 8045<br>. 813<br>. 8175<br>. 8175<br>. 8215<br>. 8235           | 33<br>38<br>60<br>34<br>150<br>325<br>640 | 0. 805<br>. 813<br>. 8165<br>. 821<br>. 8243             | 30<br>30<br>60<br>10<br>154<br>295<br>579                        |

TABLE 6.—Third fractionation.

#### FRACTIONATION IN TUBES.

|                        |  | 119 (E  | F, 0.8195)   | . 120   | ) (D,                                   | 0.820)                                    | ).                                   | 1                                  | 21 (EF   | , 0.8                 | 21).                               | 122 (EF   | 0.8215).                           |
|------------------------|--|---|--|---|---|---|--------------------------------------|------------------------------------|--|-----------------------|------------------------------------|---|------------------------------------|
|                        |  | Specifi<br>gravity  |  | spec  |   | Cul<br>cen<br>met                         | ti-                                  |                                    | ecific<br>avity.                                       | ec                    | ubic<br>enti-<br>eters.            | Specific<br>gravity.  | Cubic<br>centi-<br>meters.         |
| A<br>B<br>C<br>D<br>EF |  | $\left\{\begin{array}{c} 0.\ 805\\ .\ 814\\ \{ \ .\ 816\\ .\ 817\\ .\ 820\\ .\ 823\end{array}\right.$ |  | 58      .8     .8     .8     .8     .8     .8     .8     .8 | 805<br>811<br>817<br>8175<br>822<br>825 |   | $33 \\ 35 \\ 53 \\ 35 \\ 165 \\ 310$ | (                                  | ). 8075<br>. 814<br>. 8182<br>. 819<br>. 822<br>. 8245 |                       | 33<br>41<br>63<br>18<br>150<br>273 | $\begin{array}{c} 0.\ 803\\ .\ 811\\ .\ 8165\\ .\ 818\\ .\ 8225\\ .\ 828 \end{array}$ | 41<br>43<br>60<br>23<br>182<br>270 |
|                        |  |   | 60   | 0   |   |   | 633                                  |                                    |  |                       | 578                                |   | 629                                |
| 0                      | 123 (D-EI  | 7,0.822).   | 124 (EF,   | 0.8225).  | 125                                     | (EF,                                      | 0.823                                | 35).                               | 126 (D   | -E]                   | F, 0.824)                          | . 127 (E  | F, 0.8255).                        |
|                        | Specific<br>gravity.   | Cubic<br>centi-<br>meters.  | Specific<br>gravity.                                     | Cubic<br>centi-<br>meters.                                  |   | ecific<br>vity.                           | Cul<br>cen<br>met                    | ti-                                | Speci<br>gravi   |                       | Cubic<br>centi-<br>meters          | specific  |                                    |
| A<br>B<br>C<br>D<br>EF | $\left\{\begin{array}{c} 0.808\\ .813\\ \{ 8178\\ .8192\\ .8233\\ .8265\end{array}\right.$ | $34\\35\\52\\42\\155\\260$  | 0. 807<br>. 8095<br>. 8175<br>. 8185<br>. 8232<br>. 8275 | 31<br>27<br>65<br>17<br>150<br>300                          |   | 804<br>813<br>8185<br>8195<br>8252<br>829 |                                      | 35<br>40<br>70<br>21<br>144<br>280 | 0. 8<br>. 8<br>. 8<br>. 8<br>. 8<br>. 8                | 14<br>20<br>21<br>253 | 35<br>35<br>60<br>20<br>170<br>300 | . 815<br>. 821<br>. 823<br>. 827  | 5 40<br>75<br>25                   |
|                        |  | 578   |  | 590   |   |   |                                      | 590                                |  |                       | 620                                | -   | 635                                |

TABLE 6.—Third fractionation—Continued.

Sufficient oil of five grades for the fourth fractionation was obtained by uniting fractions from the third, as shown in Table 7.

|      |                      |  |                                  |   | Fraction                                    | s unite                                       | ed.                                   |   |   |
|------|----------------------|--|----------------------------------|---|---|---|---------------------------------------|---|---|
| Lot. | Specific<br>gravity. | Lot.   | Grade.                           | Specific<br>gravity.  | Cubic.<br>centi-<br>meters.                 | Lot.  | Grade.                                | Specific<br>gravity.  | Cubic<br>centi-<br>meters.                                    |
| 128  | 0. 815               | $\left\{\begin{array}{c} 99\\ 101\\ 103\\ 104\\ 106\\ 108\\ 109\end{array}\right.$ | EF<br>C<br>D<br>C<br>C<br>C<br>C | $\begin{array}{c} 0.814\\ .8145\\ .815\\ .815\\ .815\\ .8145\\ .8145\\ .815\\ .8145\end{array}$ | $300 \\ 22 \\ 150 \\ 175 \\ 54 \\ 55 \\ 33$ | 100<br>101<br>104<br>105<br>107<br>108<br>111 | EF<br>D<br>C<br>C<br>C<br>C<br>C<br>C | $\begin{array}{c} 0.815\\.8145\\.8147\\.8142\\.815\\.815\\.815\\.815\\.8152\end{array}$ | 315     162     28     58     85     40     65 $     65     $ |
| 129  | . 8163               | $\left\{ \begin{array}{c} 101 \\ 102 \\ 103 \end{array} \right.$                   | EF<br>EF<br>EF                   | . 817<br>. 8157<br>. 817  | 295<br>365<br>325                           | 195<br>106<br>108                             | D<br>D<br>D                           | . 8163<br>. 816<br>. 8165   | 1,542<br>270<br>150<br>170                                    |
| 130  | . 819                | $\left\{ \begin{array}{c} 104 \\ 105 \\ 106 \end{array} \right.$                   | EF<br>EF<br>EF                   | . 819<br>. 8185<br>. 8185   | 230<br>280<br>260                           | 108<br>113<br>109                             | EF<br>D<br>D                          | . 8185<br>. 8185<br>. 8185  | 1,575<br>255<br>150<br>140<br>1,315                           |
| 131  | . 8205               | $\left\{\begin{array}{c} 107 \\ 110 \\ 111 \\ 111 \\ 119 \end{array}\right.$       | EF<br>D<br>EF<br>EF              | . 8195<br>. 8195<br>. 8205<br>. 8205  | 300<br>145<br>290<br>152                    | 115<br>116<br>118                             | D<br>D<br>D                           | . 820<br>. 8205<br>. 821  | 1,313<br>130<br>160<br>154<br>1,467                           |
| 132  | . 823                | $\Big\{ { 113 \\ 115 \\ 119 } \Big\}$  | EF<br>EF<br>EF                   | . 8225<br>. 8225<br>. 823   | 283<br>300<br>300                           | 120<br>121<br>122                             | D<br>D<br>D                           | . 822<br>. 822<br>. 8225  | 165<br>150<br>182   |
|      |                      |  |                                  |   |   |   |                                       |   | 1,380   |

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TABLE 7.—Products of three fractionations united for the fourth fractionation.

The results of the fourth fractionation are stated in Table 8.

|                        | 228<br>(C-EF, 0.815).                               |   | 129<br>(D-EF, 0.8168).                                 |   | 13<br>(D-EF,   |   | 13<br>(D-EF,   |   | 132<br>(D-EF, 0.823).                              |   |
|------------------------|---|---|--|---|--|---|--|---|--|---|
|                        | Specific<br>gravity.                                | Cubic<br>centi-<br>meters.                | Specific<br>gravity.                                   | Cubic<br>centi-<br>meters.                | Specific<br>gravity.                                     | Cubic<br>centi-<br>meters.  | Specific<br>gravity.                                   | Cubic<br>centi-<br>meters.                                      | Specific<br>gravity.                               | Cubic<br>centi-<br>meters.                |
| A<br>B<br>C<br>D<br>EF | 0.8135<br>.815<br>{ .8118<br>.813<br>.8147<br>.8175 | 19<br>27<br>50<br>15<br>140<br>360<br>611 | 0. 812<br>. 8122<br>. 8165<br>. 818<br>. 818<br>. 8195 | 30<br>42<br>55<br>25<br>160<br>305<br>617 | 0. 8115<br>. 8127<br>. 8173<br>. 8185<br>. 820<br>. 8215 | $ \begin{array}{r}     24 \\     35 \\     60 \\     22 \\     160 \\     310 \\     \hline     611 \end{array} $ | 0. 8095<br>. 813<br>. 819<br>. 8195<br>. 8215<br>. 824 | 18     26     45     17     130     340     576 $     576     $ | 0.8092<br>Lost.<br>.8195<br>.8213<br>.8235<br>.826 | 35<br>35<br>60<br>25<br>150<br>280<br>585 |

TABLE 8.—Fourth fractionation.

To better compare the oils of different specific gravities that were obtained by the process just described each of six 300 cubic centimeter samples (five of partly refined oil and one of crude petroleum) was separated by distillation into ten fractions. Each sample was distilled in the same 500 cubic centimeter distilling bulb, which was heated by an electric stove that entirely surrounded it. The oil was first heated to 200° under atmospheric pressure and then to 360° under a pressure of 50 millimeters. The diminished pressure was obtained with a large Chapman water pump and kept constant by the use of a valve which automatically admitted air to the evacuated system whenever the pressure fell below 50 millimeters. This valve was constructed from a piece of iron pipe 1 inch in diameter and 5 feet long. The lower end was closed with a cap and the pipe filled with mercury to a depth of 76 centimeters. The upper end of the pipe was closed with a two-hole rubber stopper. In one hole was a long glass tube with the lower end beveled, which reached to the bottom of the mercury and could be raised or lowered as the barometer varied from day to day. In the other hole was a tube which passed just through the stopper and was connected on the outside with the apparatus to be exhausted. To prevent mercury from being drawn up and over into the apparatus by the air admitted, the end of the tube inside the stopper was drawn out and bent at a right angle and over this was slipped a cap made of larger tubing closed at the bottom, but having a fine opening in the side for air. This cap was about 6 centimeters long and extended about 3 centimeters below the end of the tube inside. If any mercury passed through this first fine opening into the cap, it would fall to the bottom without being drawn over into the apparatus or clogging the fine opening in the tube leading thereto. With this valve there was no difficulty in keeping a pressure of 50 millimeters constant within 1 millimeter.

Each distillate of sufficient volume, which was not too viscous or partly solid, was tested as to specific gravity, viscosity, and percentage absorbed when treated with concentrated sulphuric acid (specific gravity 1.84).

|   | 1.  | 2.  | 3.  | 4.   | 5.  | 6.   |
|---|---|---|---|--|---|--|
| Specific gravity<br>Viscosity.<br>Tubes passed through  |   | 0.808<br>0.0555<br>3  | 0.815<br>0.0589<br>3  | 0 8195<br>4  | 0.824<br>0.0657<br>4  | 0.810<br>0.0441<br>Crude<br>oil.   |
| Normal pressure:  |   |   |   |  |   |  |
| Below 150°. Specific gravity.<br>Viscosity.<br>Acid treatment Specific gravity.   | $\begin{array}{c} 4.4 \\ 0.722 \end{array}$                               | 1   | 13<br>0.737<br>0.0059<br>0.7365                                 | . 5  |   | 45<br>0.714<br>0.0047<br>8.6<br>0.712  |
| Amountcubic contineters<br>Specific gravity<br>Viscosity<br>Acid treatment {Per cent absorbed<br>Specific gravity                         | 47<br>0.749<br>0.0075<br>3.4<br>0.749                                     | 61<br>0.7465<br>0.0073<br>4.4<br>0.7469   | $52 \\ 0.756 \\ 0.0075 \\ 8.2 \\ 0.750 \\ \end{array}$          | 0.757<br>0.0073<br>11.3<br>0.749   | $\begin{array}{r} 60 \\ 0.759 \\ 0.0072 \\ 12.0 \\ 0.750 \end{array}$         | $\begin{array}{r} 43 \\ 0.759 \\ 0.0076 \\ 9.3 \\ 0.752 \end{array}$             |
| 50 mm. pressure:<br>[Amountcubic centimeters  | 10  | 9   | 3   | 6  | 10  | 19   |
| Specific gravity  |   |   |   |  |   | $0.7805 \\ 0.0112 \\ 11.9$   |
| Below 140° Viscosity<br>Acid treatment {Per cent absorbed<br>Specific gravity<br>Amountcubic centimeters<br>Specific gravity<br>140°-200° | 69  | 75<br>0.790<br>0.0185   | 80<br>0.797<br>0.0211   | 80<br>0.800<br>0.0216  | 73<br>0.8015<br>0.0196  | 0.7735<br>48<br>0.804<br>0.0254  |
| Acid treatment {Per cent absorbed<br>Specific gravity<br>(Amountcubic centimeters   | 3.4<br>0.790<br>25  | 0.0185<br>4.4<br>0.7885<br>30   | 8.9<br>0.7915<br>23   | . 9.6<br>0.795<br>25   | $\begin{array}{c} 14.8 \\ 0.7915 \\ 30 \end{array}$                           | 11.0<br>0.799<br>21  |
| 200°-230°   |   | 0.8135<br>0.0594<br>4.3   | $\begin{array}{c} 0.818 \\ 0.0573 \\ 11.0 \\ 0.010 \end{array}$ | 0.8225<br>0.0661<br>8.4  | $\begin{array}{c} 0.822 \\ 0.0505 \\ 10.5 \\ 0.012 \end{array}$               | 0.823<br>0.0593<br>8.7   |
| Acid treatment {Per cent absorbed<br>Amount   | $\begin{array}{c} 0.813\\ 23\\ 0.8255\\ 0.1106\\ 3.4\\ 0.8255\end{array}$ | $\begin{array}{c} 0.8125 \\ 27 \\ 0.826 \\ 0.1150 \\ 8.5 \\ 0.8255 \end{array}$ | 0.816<br>23<br>0.830<br>0.1116<br>7.0<br>0.828                  | $\begin{array}{c} 0.8217 \\ 20 \\ 0.833 \\ 0.1168 \\ 8.8 \\ 0.832 \end{array}$ | $\begin{array}{c} 0.818 \\ 24 \\ 0.838 \\ 0.1259 \\ 7.6 \\ 0.833 \end{array}$ | $\begin{array}{r} 0.8175 \\ 22 \\ 0.8355 \\ 0.1284 \\ 12.6 \\ 0.830 \end{array}$ |
| Amountcubic centimeters<br>200°-300°Specific gravity<br>Viscosity   | 20<br>0.8395<br>0.2520  | 22<br>0.838   | 23<br>Fluid.  | 24<br>Fluid.   | 20<br>Fluid.  | 17<br>Fluid.   |
| Amountcubic centimeters.  | 25  | a 30  | 27  | 30   | 26<br>Solid   | 25   |
| 340°-360°   | 0.847<br>21<br>Fluid.   | 0.849<br>a 26<br>Fluid.   | Solid.<br>22<br>Fluid.  | Solid.   | Solid.<br>19<br>Fluid.  | Solid.<br>20<br>Fluid.   |
| Residue {Amountcubic centimeters<br>Specific gravity  | 22<br>Fluid.  | 17<br>Fluid.  | 30<br>Fluid.  | 45<br>Fluid.   | 35<br>Fluid.  | 32<br>Fluid.   |
| Total volumecubic centimeters   | 298   | 298   | 296   | 295  | 299   | 292  |

| TABLE 9.—Fractionation | ı of | six | samples | by | distillation. |
|------------------------|------|-----|---------|----|---------------|
|------------------------|------|-----|---------|----|---------------|

#### *a* To 355°.

Viscosity was measured by taking the time of flow of a measured volume of oil through a capillary, the viscometer used being the one described by Ostwald and Luther as modified by Jones and Veazey.<sup>a</sup> The capacity of the small bulb was 4.5 cubic centimeters and the diameter of the capillary such as to require from five to eight minutes for that amount of oil to flow through it, and 1 minute 2.6 seconds for the same amount of water. The viscosity as well as the specific gravity was always measured at a temperature of 20° C. Viscosities have been calculated from the formula  $\eta = \eta_o \frac{TS}{T_o S_o}$  in which  $\eta_o$  is the coef-

"Zeitschr. physikal. Chemie, vol. 61, p. 651.

ficient of viscosity for water,  $S_o$  is the specific gravity of water, and  $T_o$  the time of flow of water through any given capillary at a given temperature;  $\eta$  is the viscosity coefficient of the solution investigated, S is its specific gravity as compared with water as unity at

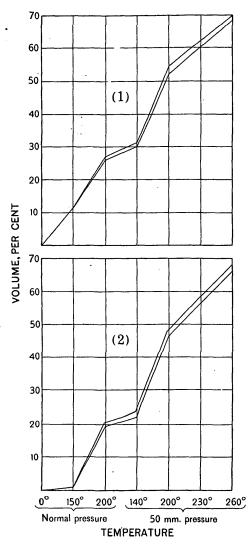


FIG. 1.—Curves showing proportion of hydrocarbons soluble in sulphuric acid, oils 1 and 2.

of these milky oils was read, their specific gravity was taken, and then the milkiness was removed by shaking and heating to about  $60^{\circ}$  with CaCl<sub>2</sub>. The specific gravity of the clear oil was then taken and the proper correction made to the milky volume. In no case,

aPhil. Trans., vol. 185A, 1894, p. 397.

any given temperature, and T is the time of flow of the given solution at that temperature. The value for pure water at  $20^{\circ}$  was taken from the work of Thorpe and Rodger.<sup>*a*</sup>

Thirty cubic centimeters of each of these distillates where that much oil was available, or all the oil there was where the volume was less than 30 cubic centimeters was mixed with an equal volume of concentrated sulphuric acid (specific gravity 1.84) and shaken for half an hour or longer in a shaking machine. The oil and acid were then poured into a separating funnel and the acid drawn off. The oil was then washed twice with water, once with aqueous NaOH, again with water, and then with this last wash water poured into a burette and allowed to settle. After standing overnight the volume was read.

The oils boiling below 200° (at 50 millimeters pressure) separated clear, but the heavy distillates were milky from water. The volume however, was this correction large, and only for the three or four heaviest oils did it exceed one-half of 1 per cent, the largest correction of all being 2.6 per cent for the distillate between  $230^{\circ}$  and  $260^{\circ}$ of the oil of specific gravity 0.824. An attempt to treat with acid

the oils selected to be distilled resulted in so much loss from the formation of emulsions that the loss in volume and change in specific gravity could not be determined with any degree of accuracy.

The results of the distillation of these samples are summarized in Table 9.

"Fluid" means that the oil at 20° was partly solid, but would flow when the bottle was inclined; "solid" means that the oil would not change its shape when the bottle was turned upside down.

It was hoped that sulphuric acid of the strength used would dissolve only unsaturated hydrocarbons and leave untouched the paraffins and benzene. By longcontinued shaking at ordinarytemperatures.however. with acid of this strength benzene is dissolved, provided that the acid is in large excess. On being shaken for four hours 100 cubic centimeters of benzene was completely dissolved in 434 cubic centimeters of acid.

Three of the distillates

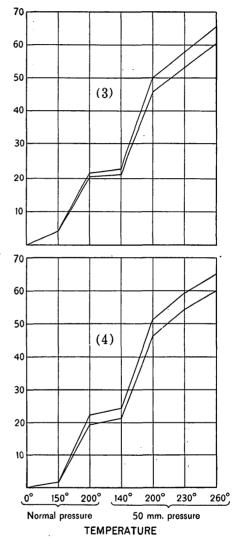
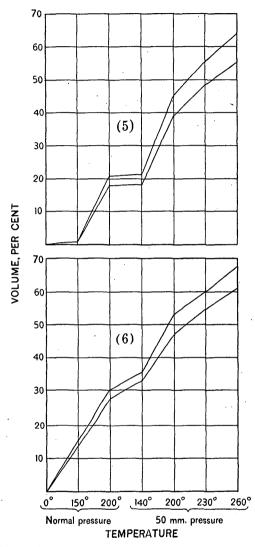
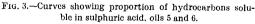


FIG. 2.—Curves showing proportion of hydrocarbons soluble in sulphuric acid, oils 3 and 4.

which had been shaken with acid showed no action when treated with a mixture of equal parts of concentrated sulphuric acid and fuming nitric acid, whereas this nitrating mixture did act on distillates which had not been previously shaken with sulphuric acid. The action of the sulphuric acid, therefore, appears to have been complete. The results of the acid treatment showed that over 90 per cent of the oil used consisted of paraffin hydrocarbons, and that in the filtration through earth the paraffin hydrocarbons tended to collect at the top of the tube and the unsaturated hydrocarbons at the bottom.





The area between the two curves represents the proportion of hydrocarbons soluble in sulphuric acid. It will be seen that this is greatest for the oils of highest specific gravity.

Tables 4 and 6 show that in several tubes the specific gravity of the oil of grade A was greater than that of the grade B oil and in some

The increasing amount dissolved by sulphuric acid in the heavier oils may be seen in the curves shown in figs.1 to 3. The abscissas represent temperatures and the ordinates volumes. The same distance on the x axis is taken to represent a distillate, whatever be the number of degrees over which it may have been collected. The upper curve represents the percentage of the total volume that distilled between given temperatures; the lower curve the percentage of the total volume recovered that was not absorbed by sulphuric acid (that is, the paraffin hydrocarbons). For the upper curve the ordinates are obtained by dividing the number of cubic centimeters in the distillate by the total volume of oil recovered. For the lower curve the ordinates are obtained by dividing the number of cubic centimeters in the distillate not absorbed by sulphuric acid by the total volume of oil recovered.

tubes than that of the grade C oil. This irregularity was marked in tubes 48, 62, 68, 72, 74, and 80 of Table 4 and 112 and 114 of Table 6. A slight irregularity appears in tubes 20, 21, 24, 27, 40, 71, and 85 of Table 4 and tube 99 of Table 6. Of the oils in these tubes that were not colorless the color was strongest where the specific gravity was greatest, so that although the oil of grade A had passed through the most earth it was yet more strongly colored than that of grade B or C.

No reason for this variation has been established. It should be remembered, however, that the different oils rise in the earth with differing velocities, not because they differ from one another in specific gravity, but because they differ in surface tension. A rough attempt was made to determine relative surface tensions by measuring the height to which different oils rise in the same capillary tube, but although a kathetometer was used and the level of the oil in the capillary brought to the same spot each time the work sufficed only to show that the difference in the surface tension of the oils was so slight as to require very careful measurement to obtain results of any value.

That the viscosity shows the same irregularity in these oils as color and specific gravity appears from the following measurements:

|    | 6:   | 2.   | 6  | 8.  |
|----|--|--|--|---|
|    | Specific<br>gravity.   | Viscos-<br>ity.  | Specific<br>gravity.                             | Viscos-<br>ity.                                     |
| AB | 0.8155<br>.808<br>.8095<br>.812<br>.8175<br>.8182<br>.8182<br>.823 | $\begin{array}{c} 0.0539\\ .0469\\ .0509\\ .0555\\ .0525\\ .0525\\ .0535\\ .0612\end{array}$ | 0.8205<br>.8043<br>.810<br>.812<br>.817<br>.8225 | 0.0626<br>.0469<br>.0520<br>.0554<br>.0524<br>.0606 |

TABLE 10.—Specific gravity and viscosity of fractions from tubes 62 and 68.

Tube 50 (Table 4) showed an irregularity in grade B, which is also found in the viscosity:

TABLE 11.—Specific gravity and viscosity of fractions from tube 50.

|    | Specific<br>gravity.   | Viscos-<br>ity.  |
|----|--|--|
| AB | $\begin{array}{c} 0.8105 \\ .8148 \\ .810 \\ .815 \\ .819 \end{array}$ | $\begin{array}{c} 0.\ 0532\\ .\ 0559\\ .\ 0526\\ .\ 0526\\ .\ 0552\end{array}$ |

The oils obtained by one fractionation of the crude petroleum (see Table 1) had the following viscosities:

1

|                             | 1  | • ,   | 2   | •   | 3.   |   |
|-----------------------------|--|---|---|---|--|---|
|                             | Specific gravity.  | Viscos-<br>ity.   | Specific<br>gravity.  | Viscos-<br>ity.   | Specific<br>gravity.                                     | Viscos-<br>ity.   |
| A<br>B<br>C<br>D<br>F<br>F. | $\left\{\begin{array}{c} 0.796\\ .808\\ .8125\\ .8137\\ .8137\\ .815\\ .818\\ .8205\end{array}\right.$ | 0. 0376<br>. 0529<br>. 0501<br>. 0529<br>. 0529<br>. 0504<br>. 0521 | 0.8012<br>.804<br>.807<br>.809<br>.8125<br>.8185<br>.8185<br>.823 | 0. 0408<br>. 0485<br>. 0443<br>. 0476<br>. 0460<br>. 0537 | 0.8022<br>.803<br>.8075<br>.810<br>.812<br>.8175<br>.821 | 0. 0401<br>. 0470<br>. 0453<br>. 0471<br>. 0472<br>. 0529 |

TABLE 12.—Specific gravity and viscosity of fractions from tubes 1 to 3.

That the viscosity does not increase with the specific gravity, particularly in the higher fractions, is apparent in two of the three series just given. The same is also shown in four tubes whose records are given in Table 4.

TABLE 13.—Specific gravity and viscosity of fractions from tubes 21, 22, 47, and 53.

|                        | 21.  |   | 22.   |   | 47   | 7.  | 53.                                     |   |
|------------------------|--|---|---|---|--|---|---|---|
|                        | Specific<br>gravity.                                   | Viscos-<br>ity.   | Specific<br>gravity.                          | Viscos-<br>ity.                                 | Specific<br>gravity.                       | Viscos-<br>ity.                                 | Specific<br>gravity.                    | Viscos-<br>ity.                                 |
| A<br>B<br>C<br>D<br>EF | 0.8038<br>8035<br>8035<br>8052<br>.805<br>.805<br>.807 | 0. 0465<br>. 0456<br>. 0456<br>. 0485<br>. 0485<br>. 0479<br>. 0480 | 0. 7997<br>. 802<br>. 8055<br>. 8063<br>. 808 | 0. 0421<br>. 0485<br>. 0502<br>. 0496<br>. 0510 | 0. 800<br>. 807<br>. 814<br>. 816<br>. 819 | 0. 0453<br>. 0538<br>. 0542<br>. 0528<br>. 0556 | 0.803<br>.8105<br>.815<br>.8185<br>.820 | 0. 0515<br>. 0563<br>. 0684<br>. 0570<br>. 0559 |

This drop in viscosity which occurs at the bottom of the tube appears to be a regular occurrence in the dozen or so oils which have been tested. Further investigation of this point is intended.

#### WATER FRACTIONATION.

To test the effectiveness of water fractionation alone, 1,000 cubic centimeters of crude petroleum, previously chilled and filtered, of specific gravity 0.807, was mixed with 1,000 grams of earth and allowed to stand for twenty-four hours. Water was then added in small amounts and the oil collected. The results are stated below.

|    | Specific<br>gravity.                                    | Cubic<br>centi-<br>meters.                | Total<br>water<br>present<br>(cubic<br>centi-<br>meters). |
|----|---|---|---|
| AB | 0. 8148<br>. 8139<br>. 816<br>. 820<br>. 8225<br>. 8245 | 44<br>278<br>211<br>84<br>28<br>28<br>673 | 500<br>650<br>800<br>950<br>1,400<br>2,750                |

TABLE 14.—Fractionation of crude petroleum with water.

 $\mathbf{28}$ 

The fractions of large enough volume were then mixed with earth again and the oil replaced with water. One gram of earth was used for each cubic centimeter of oil, the earth having been heated and allowed to cool. Table 15 shows the results.

|   | В.  |   |   | с.   |  |   | D.                                    |  |  |
|---|---|---|---|--|--|---|---------------------------------------|--|--|
| Specific<br>gravity<br>Cubic cen-<br>timeters.<br>Time (hrs.) | 278   |   |   | 0.816<br>211<br>6  |  |   | 0.820<br>84<br>2.5                    |  |  |
| 1<br>2<br>3<br>5<br>6<br>7<br>9                               | Specific<br>gravity.<br>0.8185<br>.818<br>.818<br>.818<br>.817<br>.819<br>.820<br>.820<br>.8215 | Cubic<br>centi-<br>meters.<br>10<br>10<br>21<br>20<br>42<br>10<br>44<br>16<br>20<br>193 | Water<br>(cubic<br>centi-<br>meters).<br>70<br>110<br>164<br>216<br>277<br>428<br>686 | Specific<br>gravity.<br>0.820<br>.820<br>.8195<br>.820<br>.820<br>.820 | Cubic<br>centi-<br>meters.<br>10<br>20<br>72<br>30<br>10<br>10 | Water<br>(cubic<br>centi-<br>meters).<br>80<br>125<br>250<br>410<br>588 | Specific<br>gravity.<br>0.822<br>.823 | Cubic<br>centi-<br>meters.<br>32<br>20 | Water<br>(cubic<br>centi-<br>meters).<br>76<br>207 |

TABLE 15.—Second fractionation of petroleum with water.

It is apparent that while petroleum is fractionated by simply mixing the oil with fuller's earth and then displacing the oil from the earth with water, the fractionation is much more complete when tubes are used, as previously described.

It will be noticed that although fractions C and D of Table 14 are separated hardly at all by further treatment with earth and water (Table 15), yet the specific gravity of all the oil recovered is higher than that of the oil used; for example, fraction C (specific gravity 0.816) yields nothing lighter than 0.8195, and D (specific gravity 0.820) nothing lighter than 0.822.

To determine whether the specific gravity of the oil recovered will continue to rise after the oil is fractionated no further by repeated treatment, 330 cubic centimeters of specific gravity 0.819, obtained by uniting several products of one fractionation of the crude petroleum, were mixed with 330 grams of earth, and water was added, as shown in Table 16.

| •                                     | -<br>- |                                       | Specific<br>gravity. | Cubic<br>centi-<br>meters. | Total<br>water<br>present<br>(cubic<br>centi-<br>meters). |
|---------------------------------------|--------|---------------------------------------|----------------------|----------------------------|---|
| <u>A</u>                              |        | · · · · · · · · · · · · · · · · · · · |                      | 6                          | 64  |
| B<br>C                                |        |                                       | 0.8215               | $50 \\ 12$                 | 214   |
| D                                     |        |                                       |                      | 60                         | 270   |
| E                                     | •••••  | •••••••••••••••••                     |                      | 82<br>26                   | 413<br>613  |
| · · · · · · · · · · · · · · · · · · · | •••••• | •••••••••••••••••                     | 8220                 | 20                         | 013   |
| •                                     |        |                                       |                      | 236                        |   |

TABLE 16.—Second fractionation of petroleum (combined sample) with water.

When 75 cubic centimeters of fraction E (specific gravity 0.821) was next mixed with 75 grams of earth and 150 cubic centimeters of water was added, 51 cubic centimeters of oil whose specific gravity was unchanged, but whose color was reduced, was obtained. Fifty cubic centimeters of this oil when treated with earth and water, returned 34 cubic centimeters of oil with the color considerably lighter, but with the specific gravity still 0.821.

Although only two-thirds of the oil used is recovered when oil is mixed with earth and then displaced with water, yet this loss does not seem to affect the specific gravity of the oil obtained except in the first one or two treatments after the oil ceases to be fractionated. After these first treatments the oil recovered has the same specific gravity as the oil used.

#### OIL LOST IN THE FULLER'S EARTH.

The sum of the fractions of oil displaced from the earth is as a rule only about two-thirds of the volume of the oil used. A pressure of approximately 200 tons per square inch on the earth from which water has displaced all oil that it will results in the liberation of considerable water but very little oil. When earth which has been pressed is heated to 165° for three hours, considerable water distills over, but much less oil than would be expected; for example, from 75 grams of earth which should contain 25 cubic centimeters of oil only 4 cubic centimeters of oil was obtained. The earth was removed once from the flask and pulverized, and when the heat was discontinued the earth was thoroughly dry. On extraction with ether in a Soxlet extractor the earth gave a solution having the color of the original petroleum. The extraction was continued until the extract was colorless. On evaporation of the ether there remained about 8 cubic centimeters of a heavy oil with the color of the natural petroleum. Pressure, heat, and extraction with ether together gave about half the amount of oil which the earth must have contained.

Earth that had been used once was allowed to dry for several weeks at room temperature until it had lost all appearance of containing moisture. It was then pulverized, sifted, and 720 grams used in a tube with 740 cubic centimeters of the crude petroleum of specific gravity 0.810, with the following results:

|  | Specific<br>gravity.  | Cubic<br>centi-<br>meters.   |
|--|---|--|
| 8 centimeters at top.<br>Next 8 centimeters<br>Next 18 centimeters.<br>Next 30 centimeters.<br>Rest. | 0.8284<br>.8225<br>{ .8143<br>.8155<br>{ .8175<br>{ .8175<br>.819 | $ \begin{array}{r} 0 \\ 10 \\ 45 \\ 60 \\ 80 \\ 83 \\ 114 \\ 392 \end{array} $ |

TABLE 17.—Fractionation of crude petroleum with earth that had been used once.

The first oil up the tube is evidently absorbed by heavy material in the earth; the first oil recovered dissolves material from the earth, which increases its specific gravity beyond that of the next fraction.

To see how much of the weight of the earth used the second time was due to material which it had retained from its first use, 300 grams of earth was mixed with 300 cubic centimeters of crude petroleum and the oil displaced by water. The oil recovered measured 205 cubic centimeters, and the weight of the earth after drying for several weeks at room temperatures was 347.5 grams. Fully 15 per cent, therefore, of the weight of the earth used the second time was solid matter which it had retained from its first use.

In all tests the earth was heated before it was used because it was believed that heating decreased the amount of oil lost in the earth. The earth was heated usually in iron pans on a gas stove until it ceased to form geysers when stirred. A tube 5 feet long and  $1\frac{1}{4}$  inches in diameter, packed with 948 grams of earth that had not been heated, gave results as follows with 930 cubic centimeters of crude petroleum of specific gravity 0.810, after standing for twenty hours at diminished pressure:

TABLE 18.—Fractionation of crude petroleum with earth that had not been heated.

|                            |                   | • • . |           | gravity.                    | Cubiccen-<br>timeters. |
|----------------------------|-------------------|-------|-----------|-----------------------------|------------------------|
| Top 8 centi<br>Next 8 cent | meters<br>imeters | <br>  | <br>····· | <br>0,803<br>.8045<br>.8103 | 30<br>38<br>85         |
|                            |                   |       |           | <br>. 0100                  | 440<br>                |

In a test of water fractionation alone with unheated earth but 242 cubic centimeters of oil was recovered from 500 cubic centimeters of crude petroleum.

The results obtained toward the close of our work indicate that the loss of oil when unheated earth is used is much less than we had supposed it to be. The gain from heating the earth may not pay for the trouble of heating it, and this point should be investigated before any very extensive experiments are again undertaken.

Earth after heating must become thoroughly cold before it is used to pack tubes. The earth holds its heat for several hours, and if it is used the same day on which it is heated, there is apt to be sufficient contraction in the tube to allow the oil to run up the side as it would in a vacuum.

The length of the tubes used was  $5\frac{1}{2}$  feet. A tube 9 feet long was connected to the same vacuum pump with several  $5\frac{1}{2}$ -foot tubes and held for two days with a constant diminished pressure of about 10 centimeters Hg. The oil was drawn to the top of the shorter tubes; these were removed and a second lot substituted, and these also were fully impregnated with oil before the long tube was opened. When it was opened the oil had ascended but 45 centimeters, showing that the diminished pressure had not penetrated the 9 feet of earth and reached the bottom of the tube.

A shorter tube in which the earth was packed very much harder, so that it rang like an iron rod when pounded on the floor, was connected with a vacuum pump at one end and a manometer at the other, and showed diminished pressure on the manometer when the column of earth was 2 feet long but not when it was 2 feet 4 inches.

FRACTIONATING POWER OF SUBSTANCES OTHER THAN FULLER'S EARTH.

A clay from Topsham, Me., showed in tubes a power of fractionating as well as of decolorizing the higher fractions. Tubes 5 feet long and  $1\frac{1}{4}$  inches in diameter were used, with petroleum of specific gravity 0.806. Compared with fuller's earth, the action was as follows:

 TABLE. 19.—Fractionation of crude petroleum with clay from Topsham, Me., and with fuller's earth.

|   | Clay. | Fuller's<br>earth.  |
|---|-------|---|
| 8 centimeters at top.<br>Next 8 centimeters.<br>Next 8 centimeters.<br>Next 10 centimeters.<br>Next 30 centimeters.<br>Next 45 centimeters.<br>Time required. | do    | 0. 793<br>. 800<br>. 806<br>. 807<br>. 8092<br>. 8112<br>. 76 |

Neither powdered brick made from the same clay nor powdered feldspar showed any power of fractionation.

Another similar clay (from Mere Point, Brunswick, Me.) showed a power of water fractionation, but its behavior in a tube was not tested. Four hundred grams of this clay, previously sifted and heated, was mixed with 170 cubic centimeters of crude petroleum of specific gravity 0.806 and allowed to stand for fourteen hours. Water was then added and the following fractions were obtained:

TABLE 20.—Fractionation of crude petroleum with clay from Brunswick, Me.

|                   | Specific<br>gravity.       | Cubic cen-<br>timeters.    | Total<br>water<br>present<br>(cubic<br>centime-<br>ters). |
|-------------------|----------------------------|----------------------------|---|
| A<br>B<br>C<br>D. | 0. 8165<br>. 817<br>. 8188 | 24<br>60<br>20<br>6<br>110 | 104<br>133<br>234<br>374                                  |

The color was scarcely changed at all.

#### SUMMARY.

1. When petroleum is allowed to rise in a tube packed with fuller's earth, there is a decided fractionation of the oil, the fraction at the top of the tube being of lower specific gravity than that at the bottom.

2. When water is added to fuller's earth which contains petroleum, the oil which is displaced first differs in specific gravity from that which is displaced afterward, when more water is added.

3. When petroleum is allowed to rise in a tube packed with fuller's earth, the paraffin hydrocarbons tend to collect in the lightest fraction at the top of the tube and the unsaturated hydrocarbons at the bottom.

4. When oil is mixed with fuller's earth and then displaced with water, about one-third of the oil remains in the earth.

0